



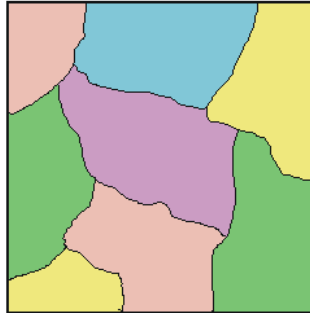
Crystallographic texture

- Introduction
- Representation of Texture
- Experimental Methods for Texture Determination
- Deformation Texture
- Annealing Texture

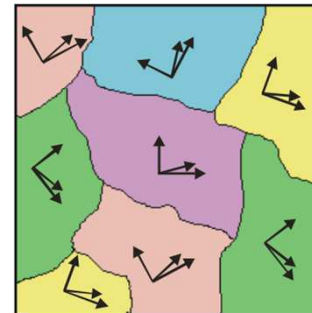


Texture and anisotropy of polycrystals

grain structure

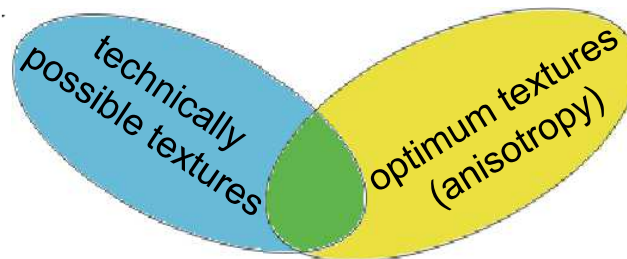


texture



texture forming processes

directional solidification
deformation
recrystallization
etc.

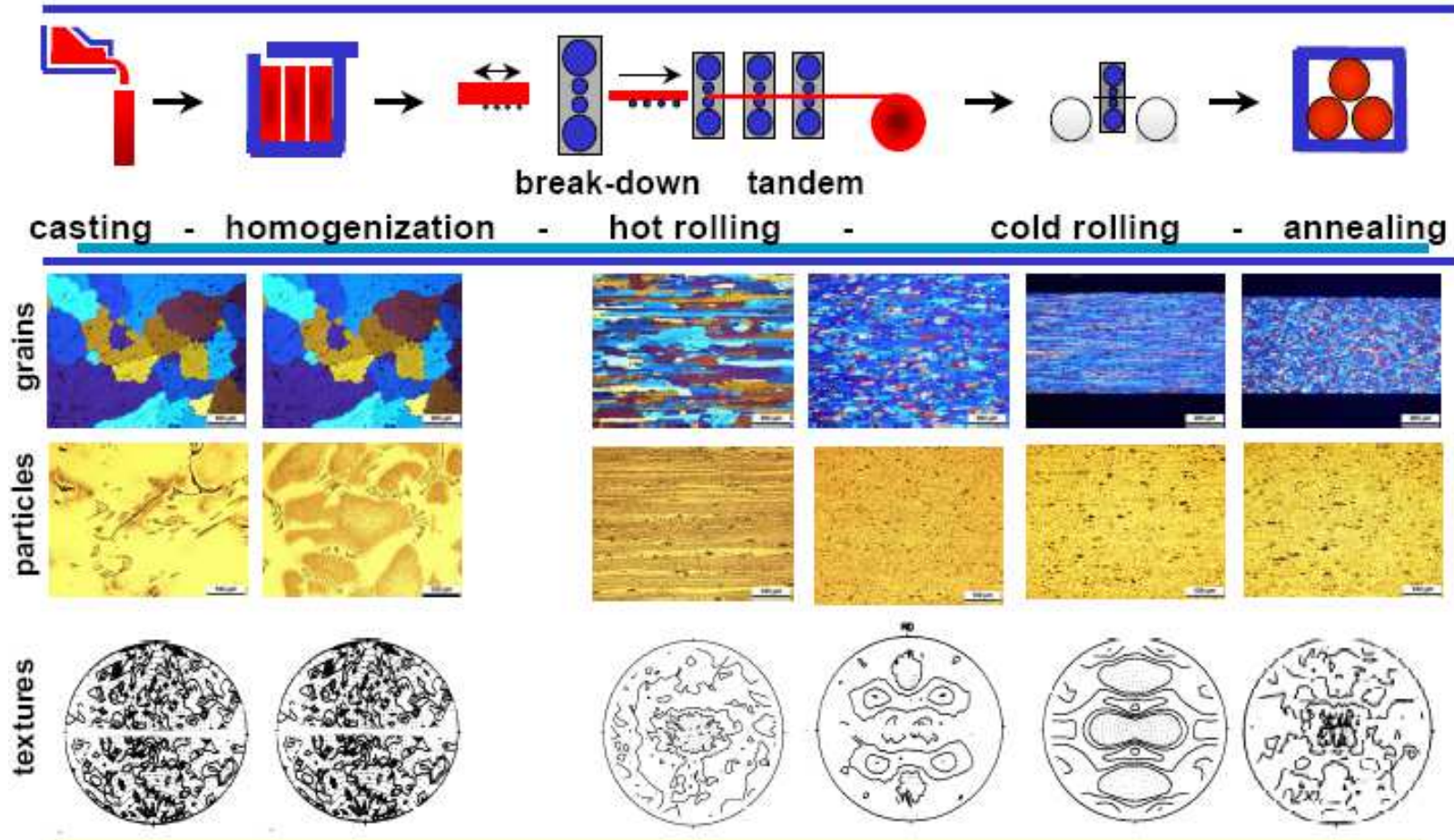


anisotropic properties

elasticity
plasticity
magnetism
etc.



Evolution of typical microstructures in industrial aluminium sheet production

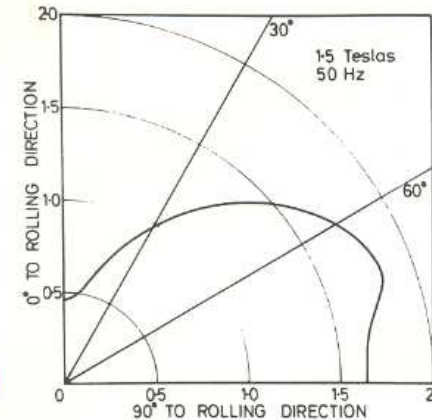




Texture and anisotropy of polycrystals

➤ Texture in polycrystalline materials is ubiquitous

- Goss oriented Silicon steel
- Earing of aluminum cans
- Substrate for semiconductor tapes
- Fatigue properties of aluminum and titanium alloys
- Quality of epitaxial films: **$\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$ Pmmm space group c_{\perp} epitaxy**
- Recoverable strain in SMA

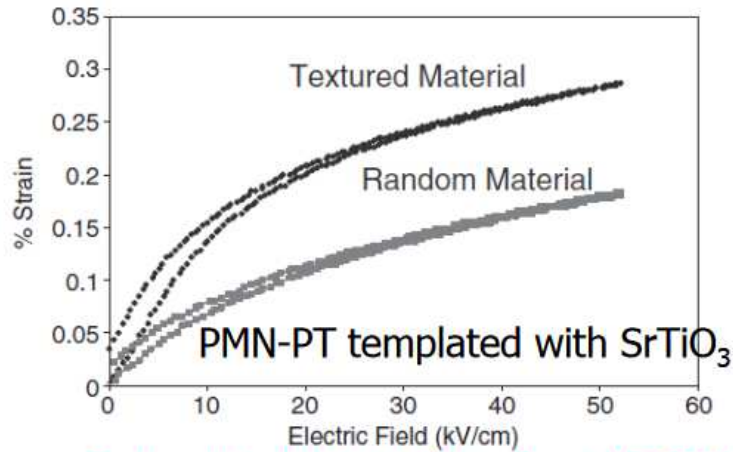




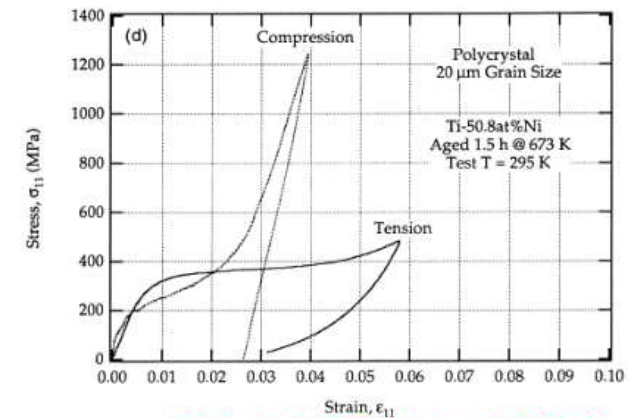
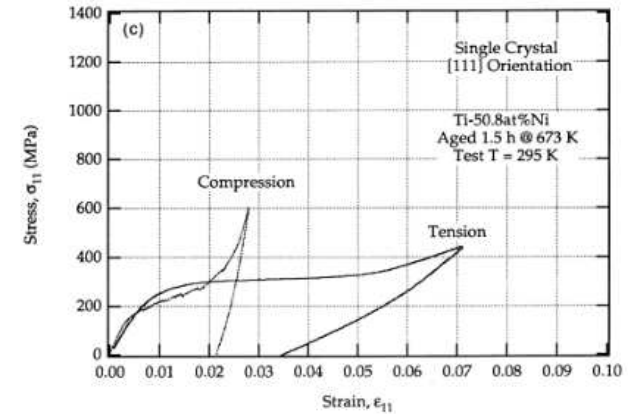
Texture and anisotropy of polycrystals



www.alumatter.org.uk



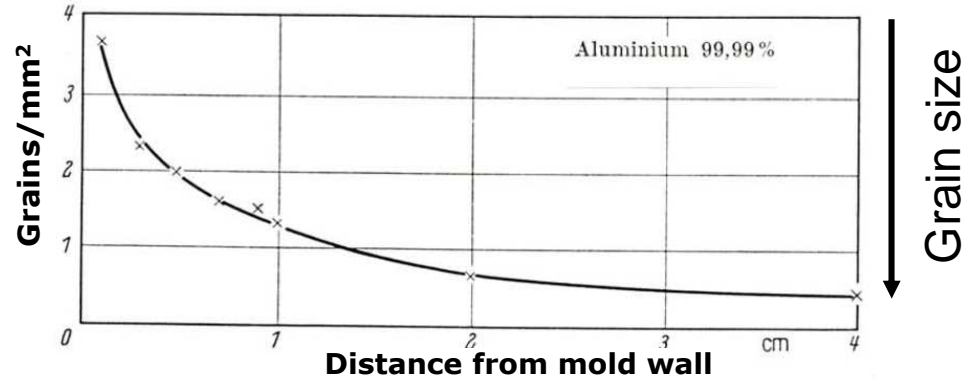
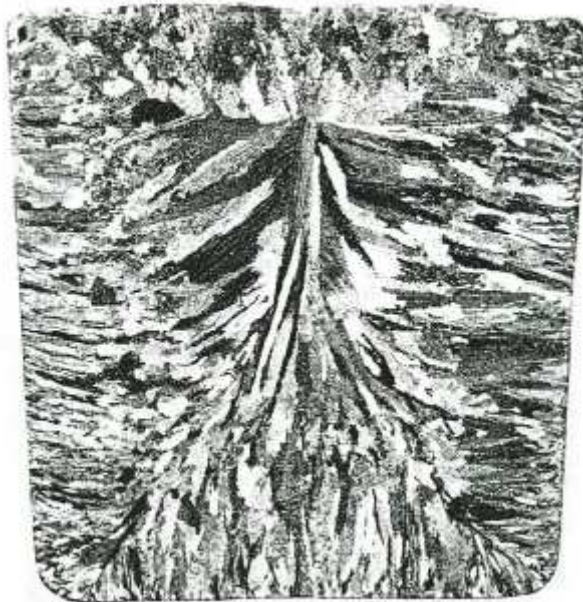
Seabaugh et al. *J. Intel. Mater. Struct.* 15 (2004)



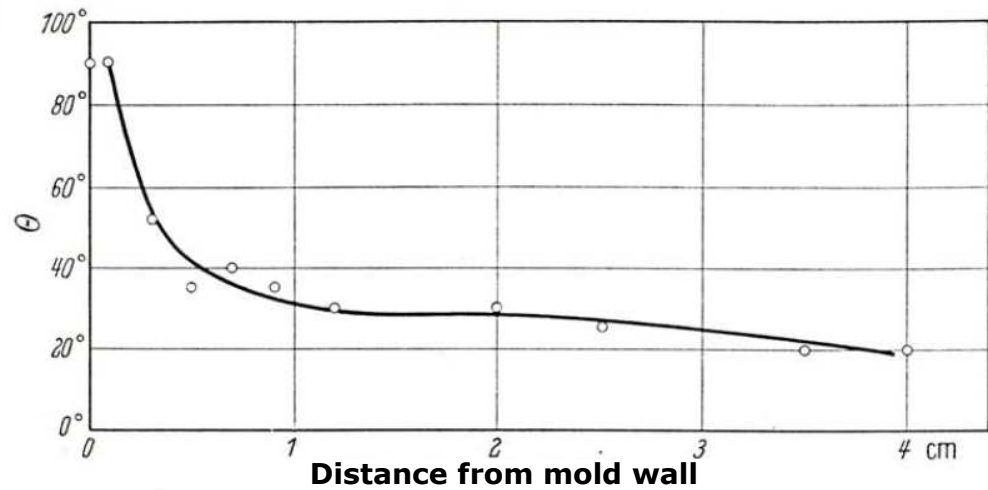
Gall et al. *Acta Mater.* 47 (1999)



Cast grain structure and cast texture



Grain size



$\Theta/2 = \text{Scatter}$
 $\langle 100 \rangle / \text{column axis}$

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Walton & Chalmers, 1959



Crystallization

Stationary melt

Requirement for growth texture:

- a) temperature gradient
- b) anisotropic crystal growth \Rightarrow growth selection

Cast texture is correlated with dendrite alignment

\Rightarrow related to dendrite formation

Requirement for dendrite formation:

thermally or constitutionally supercooled melt
ahead of growth front, negative T-gradient

Moving melt (laminar flow, e.g. magma flow)



Dendrite growth and cast texture

Tabelle 53. Zusammenhang zwischen dem dendritischen Wachstum und der Gußtextur
 (nach WALTON und CHALMERS)

Metall bzw. Legierung	struktur	Dendriten-Richtung		Gußtextur
		beobachtet	erwartet	
Fe-Si	kubisch raumzentriert		$\langle 100 \rangle$	$\langle 100 \rangle$
β -Messing	kubisch raumzentriert		$\langle 100 \rangle$	$\langle 100 \rangle$
Na	kubisch raumzentriert	$\langle 100 \rangle$	$\langle 100 \rangle$	
Al	kubisch flächenzentriert	$\langle 100 \rangle$	$\langle 100 \rangle$	$\langle 100 \rangle$
Cu	kubisch flächenzentriert		$\langle 100 \rangle$	$\langle 100 \rangle$
Ag	kubisch flächenzentriert		$\langle 100 \rangle$	$\langle 100 \rangle$
Au	kubisch flächenzentriert		$\langle 100 \rangle$	$\langle 100 \rangle$
Pb	kubisch flächenzentriert	$\langle 100 \rangle$	$\langle 100 \rangle$	$\langle 100 \rangle$
Cd	hexagonal dicht. Kugelp.		$\langle 10\bar{1}0 \rangle$	$\langle 10\bar{1}0 \rangle$
Zn	hexagonal dicht. Kugelp.	$\langle 10\bar{1}0 \rangle$	$\langle 10\bar{1}0 \rangle$	$\langle 10\bar{1}0 \rangle$
Mg	hexagonal dicht. Kugelp.		$\langle 10\bar{1}0 \rangle$	unsicher
Bi	rhomboedrisch			$\langle 111 \rangle$
β -Sn	tetragonal	$\langle 110 \rangle$	$\langle 110 \rangle$	$\langle 110 \rangle$

Wassermann
 & Grewen,
 1962



Plastic deformation

Orientation change through single slip of a single crystal

Models for deformation texture development of polycrystals:

1) Sachs (1928)

Stress equilibrium: $\sigma_g = \sigma$

⇒ slip (in general single slip) on slip system with highest Schmid factor

⇒ Formation of overlaps and pores at grain boundaries

2) Taylor (1938)

Strain compatibility: $\varepsilon_g = \varepsilon$

⇒ Activation of 5 independent slip systems (von Mises criterion)

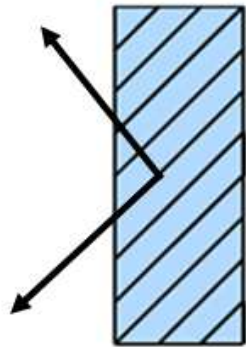
independent \equiv shape change through slip on this system should not be achieved by combined slip on other systems.

5 independent systems, because each grain should be able of a general shape change, i.e. 5 independent components of the strain tensor (ε_{ik}) should be realized through slip on slip systems.

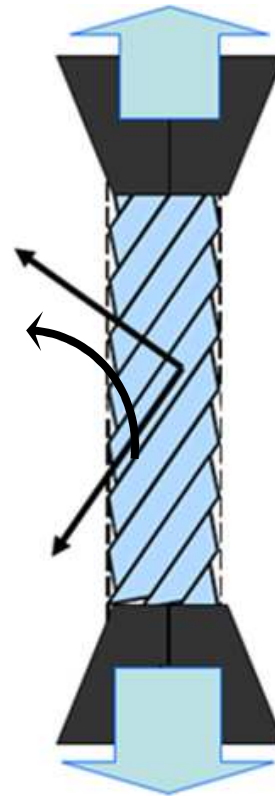
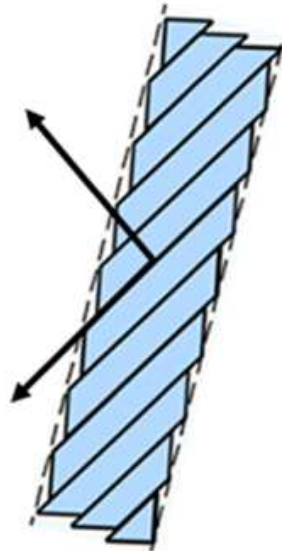


Orientation change through deformation

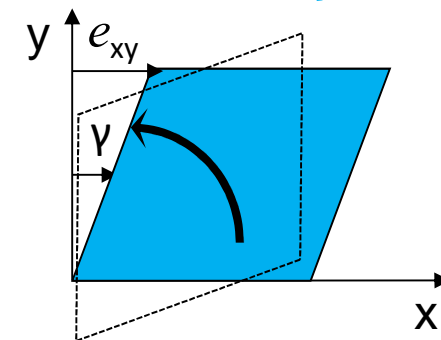
Unslipped single crystal



Slipped single crystal
without grip constraint with grip constraint



$$e_{kl} = \begin{bmatrix} e_{xx} & e_{xy} & e_{xz} \\ e_{yx} & e_{yy} & e_{yz} \\ e_{zx} & e_{zy} & e_{zz} \end{bmatrix}$$

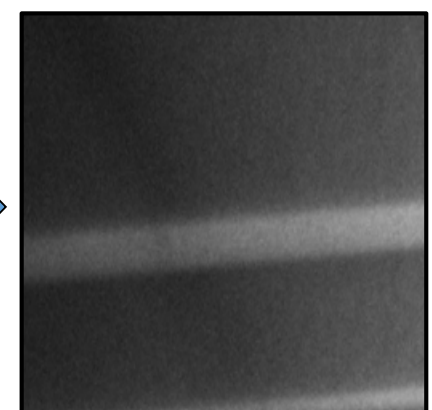
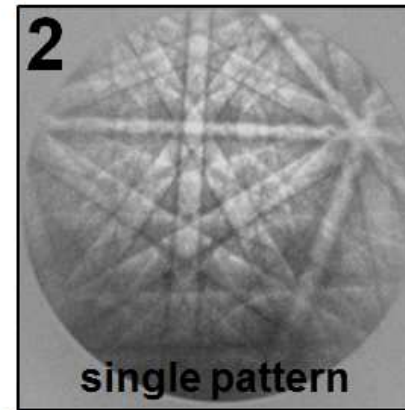
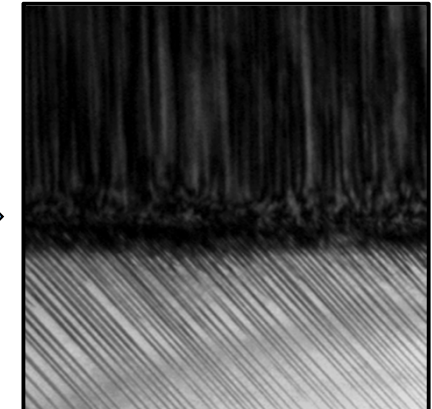
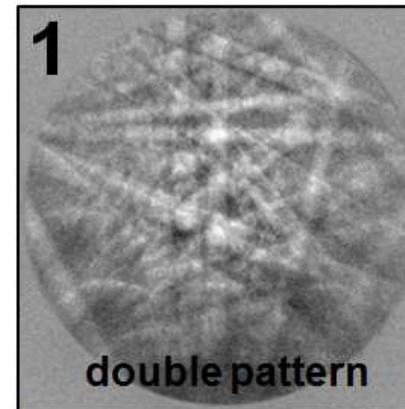
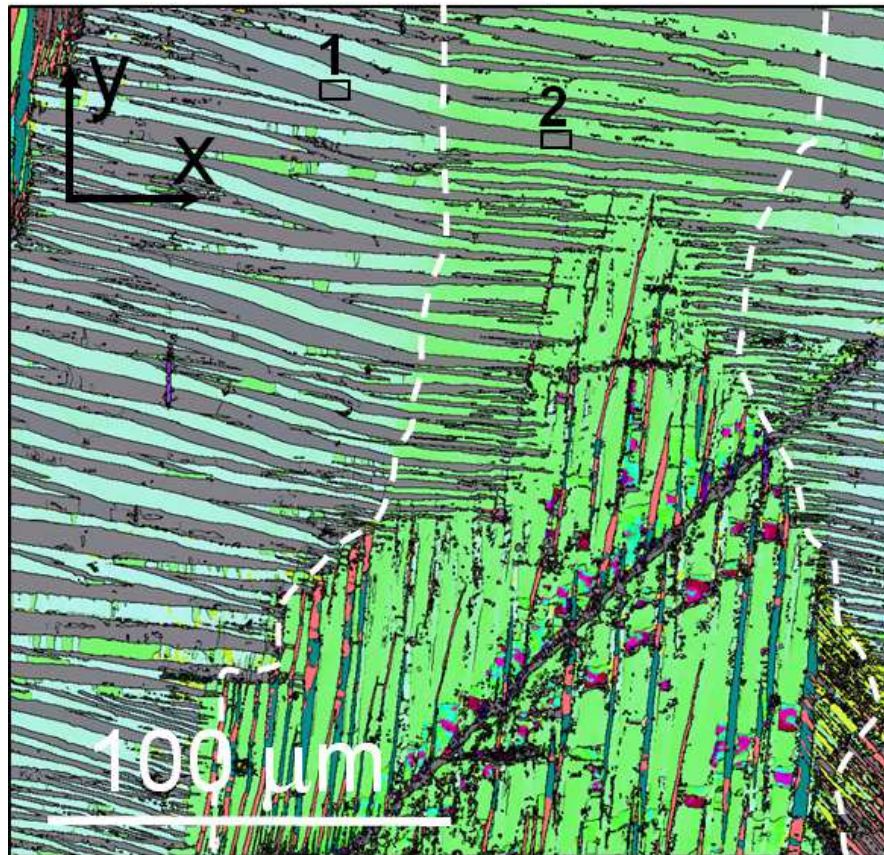


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Training procedure



EBSD mapping, All Euler color coding

Lüders type deformation

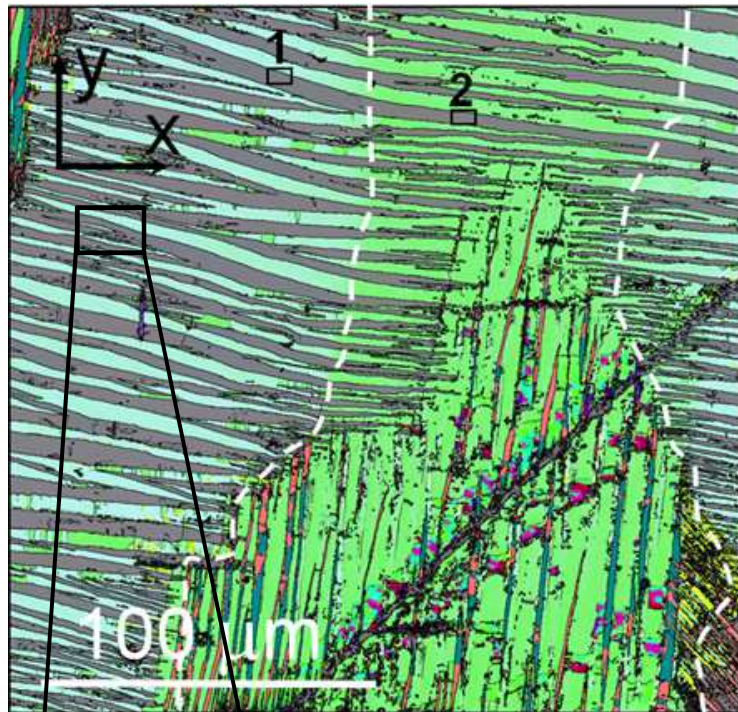
Project WND-POWR.03.02.00-00-I043/16

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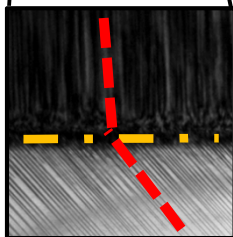
M.J. Szczerba and R. Chulist, Acta Mater. 85 (2015) 67-73
Project co-financed by the European Union within the European Social Funds



Nanotwinning

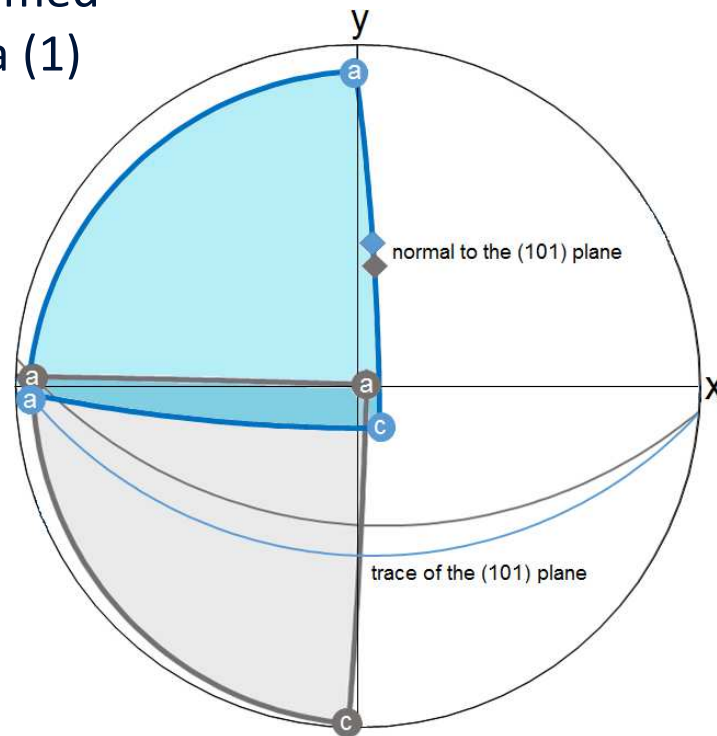


EBSD mapping, All Euler color coding

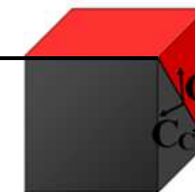


- - - inter-variant b.
- - - twin b.

undeformed
area (1)



common a-axis



twin plane (101)

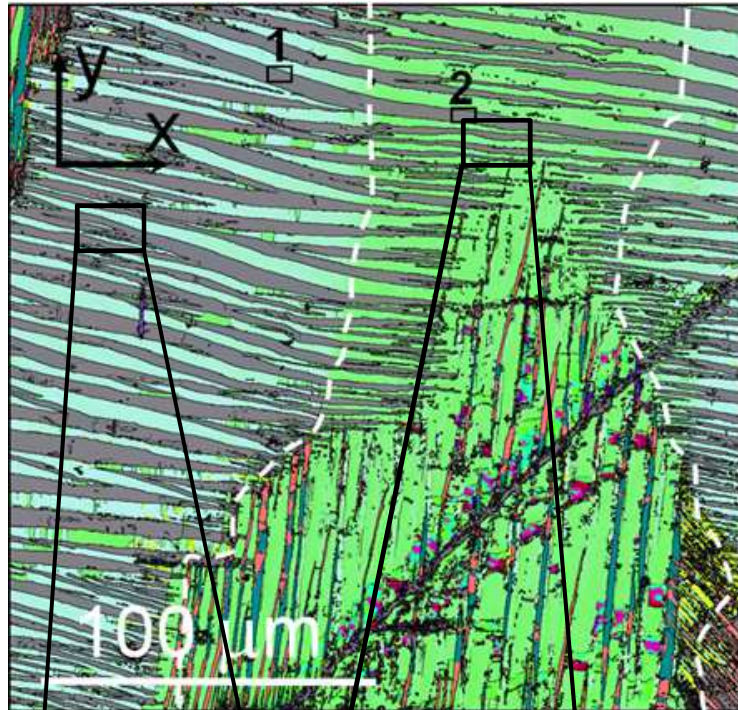
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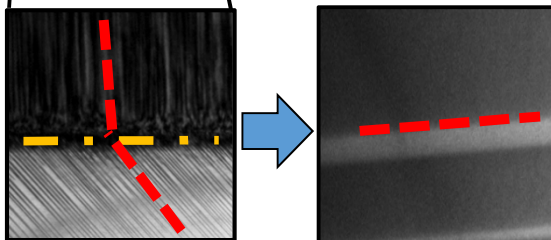
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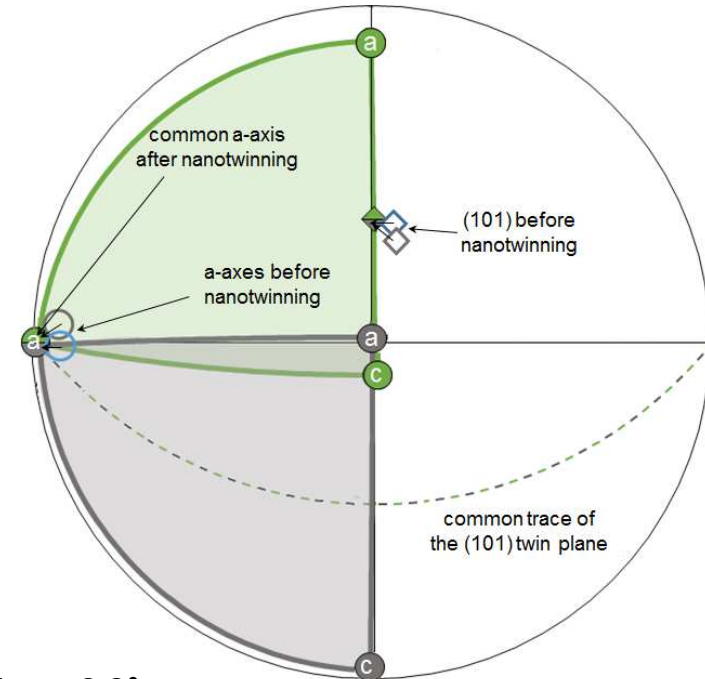
Nanotwinning



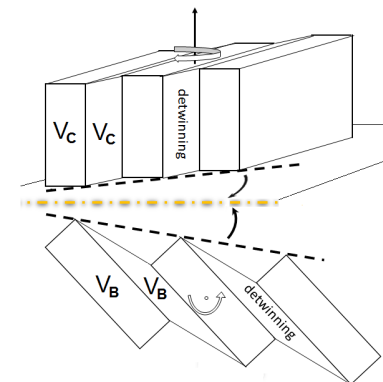
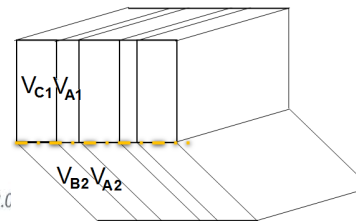
EBSD mapping, All Euler color coding



deformed
area (2)



calculated rotation = 3.3°
measured rotation = 3.4°



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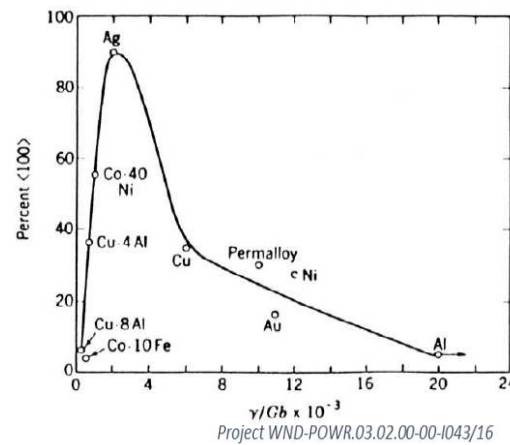
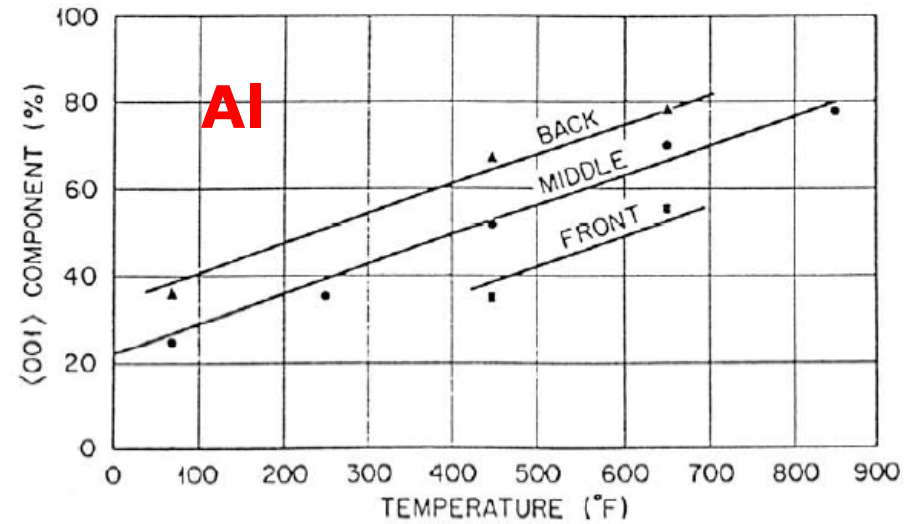
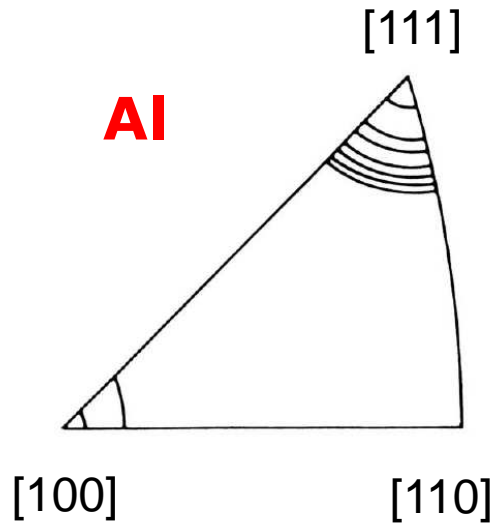
Crystallography of slip and twinning in cubic metals

Structure	Slip System	
	Plane	Direction
fcc	{111}	<110>
bcc	{110}	<111>
	{112}	<111>
	{123}	<111>

Structure	Twinning shear	Twinning Plane	Twinning Direction
fcc	0.707	{111}	<112>
bcc	0.707	{112}	<111>



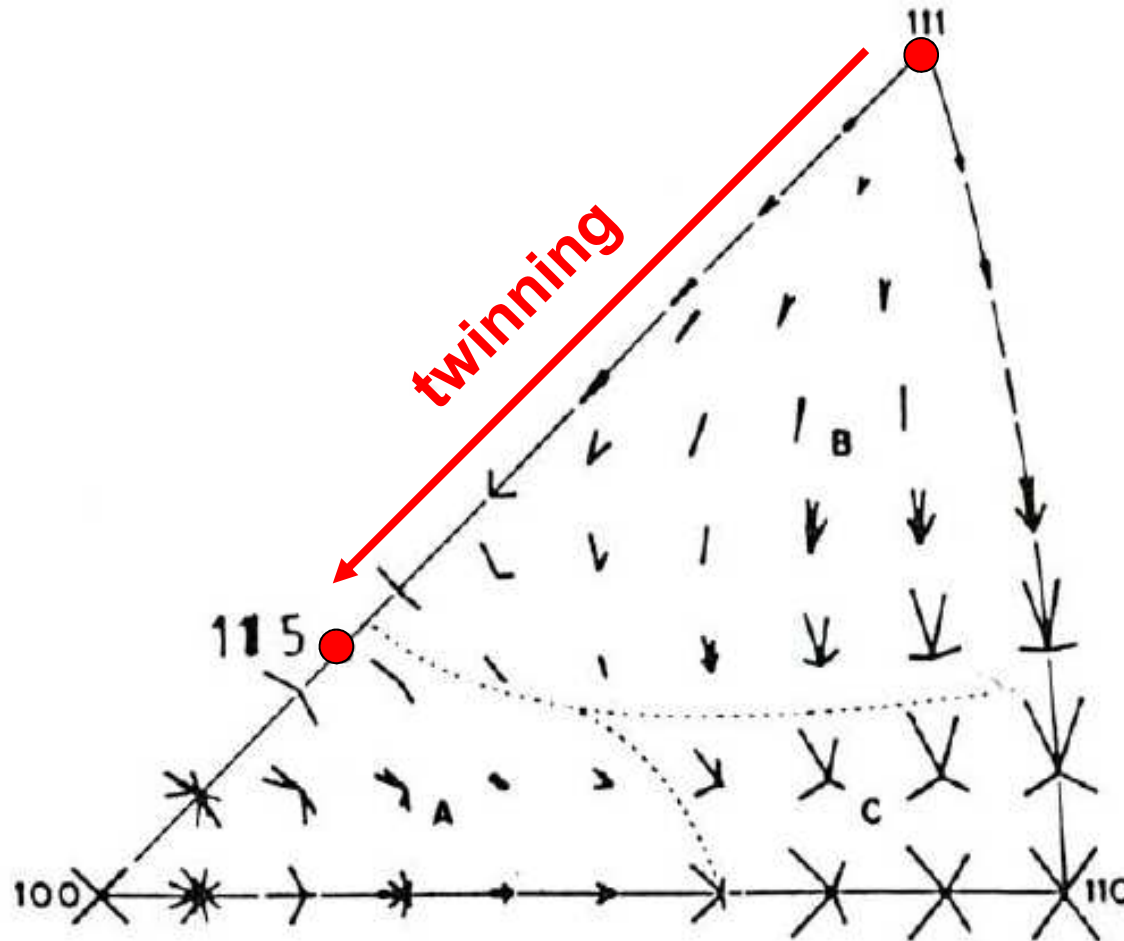
Tension textures of fcc metals



English & Chin, 1965



Orientation changes in tension (FC Taylor)



Chin et al., 1967



Young's Modulus

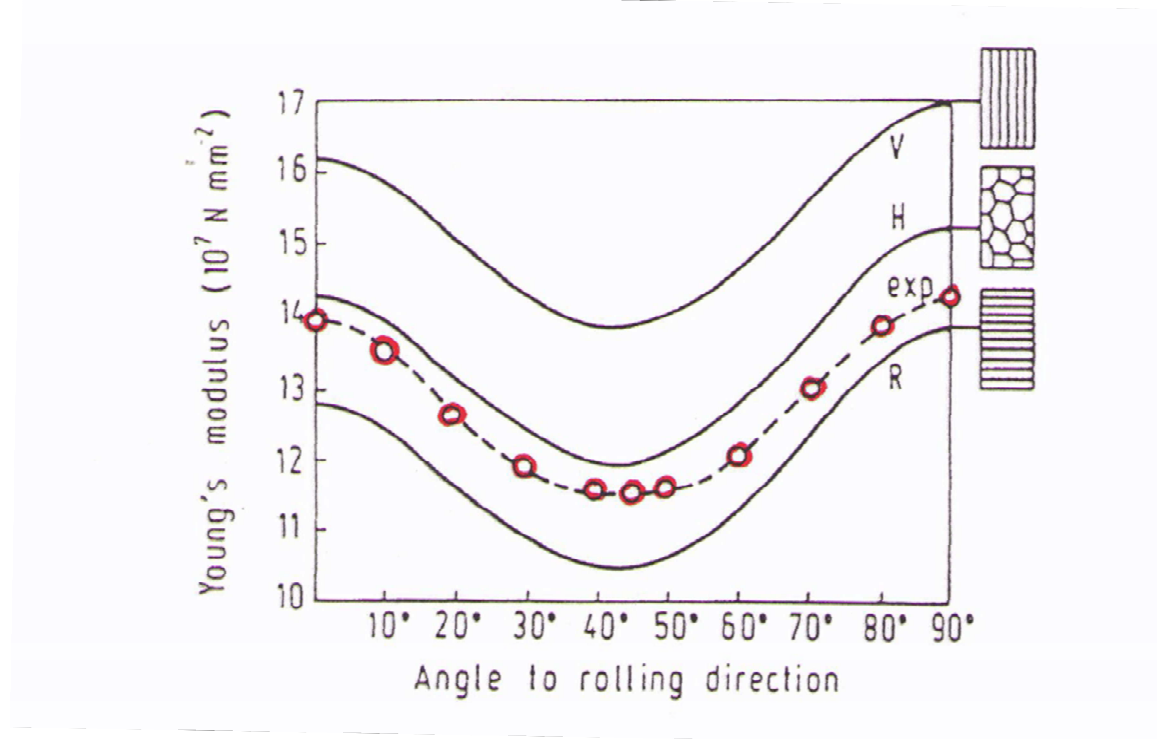
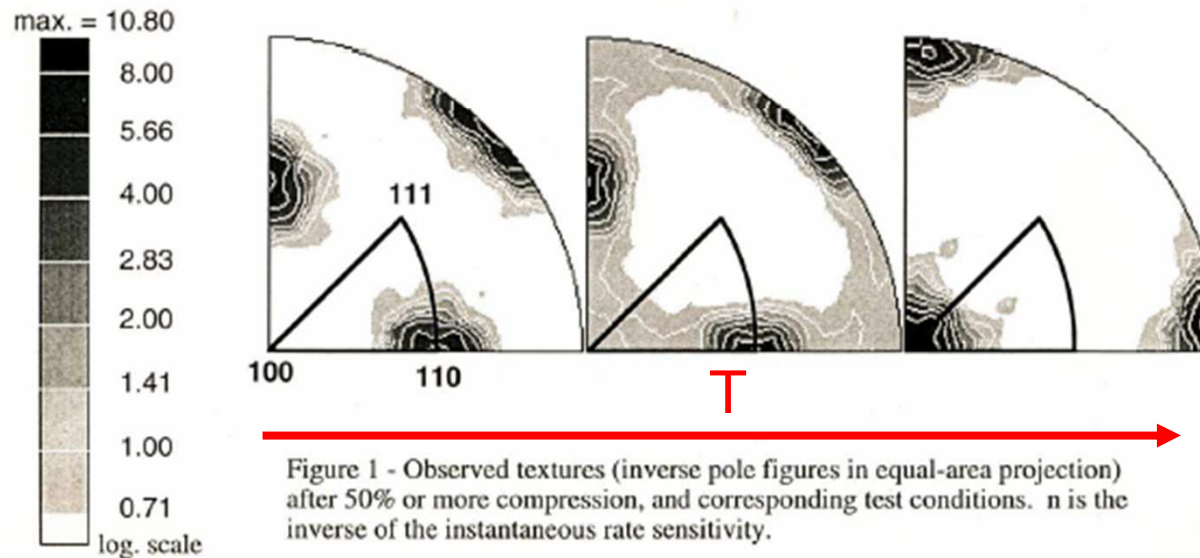


Fig. 5 Young's modulus as a function of the direction in the sheet plane for a textured copper sheet compared with the Voigt-Reuss-Hill approximations calculated from the ODF.



Compression textures of fcc metals

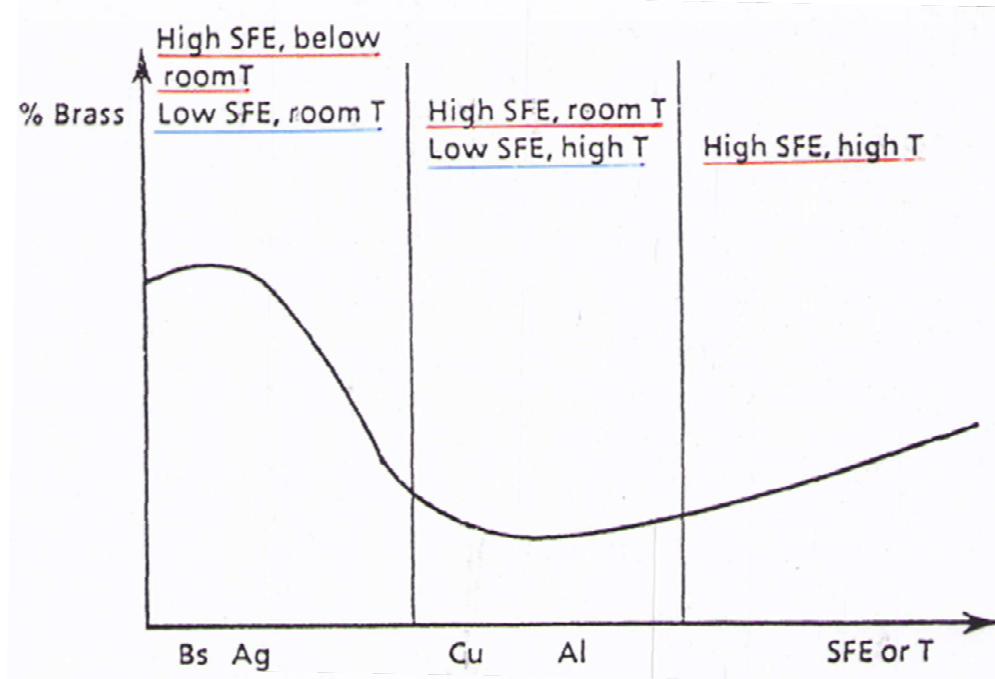
	$n \gg 4$	$n \approx 4$	$n \approx 3$
Al-2%Mg	T=25°C, $\dot{\epsilon} = 10^{-2} \text{s}^{-1}$ T=282°C, $\dot{\epsilon} = 10^{-1} \text{s}^{-1}$	T=282°C, $\dot{\epsilon} = 10^{-5} \text{s}^{-1}$ T=380°C, $\dot{\epsilon} = 10^{-3} \text{s}^{-1}$	T=360°C, $\dot{\epsilon} = 5 \cdot 10^{-5} \text{s}^{-1}$ T=440°C, $\dot{\epsilon} = 10^{-4} \text{s}^{-1}$
Al-5%Mg	T=25°C, $\dot{\epsilon} = 10^{-2} \text{s}^{-1}$ T=300°C, $\dot{\epsilon} = 5 \cdot 10^{-2} \text{s}^{-1}$	T=473°C, $\dot{\epsilon} = 1 \text{s}^{-1}$ T=380°C, $\dot{\epsilon} = 10^{-3} \text{s}^{-1}$	T=473°C, $\dot{\epsilon} = 10^{-2} \text{s}^{-1}$ T=473°C, $\dot{\epsilon} = 10^{-4} \text{s}^{-1}$ (Tension or Compression)



Kocks et al.,
1994



Deformation textures of fcc metals



	Brass-Type	Copper-Type
Tension	$\langle 100 \rangle$ fibre	$\langle 111 \rangle$ fibre
Rolling	α fibre	β fibre
Torsion	Mostly B.	Mostly C

Bacroix,
1987

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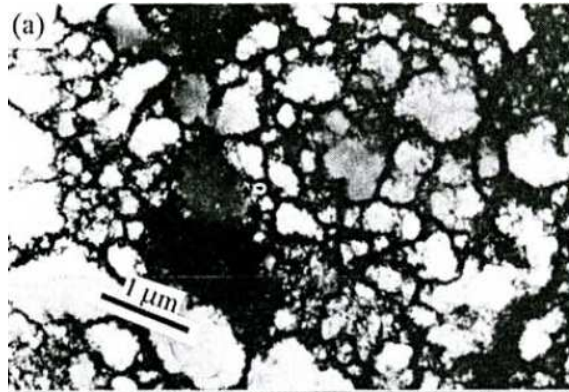


Microstructure in deformed metals (cold rolled Cu)

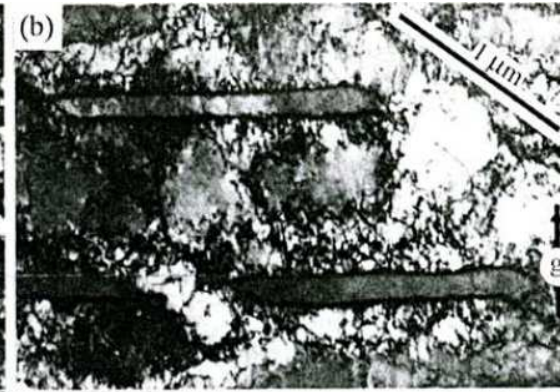
cell structure

mirobands

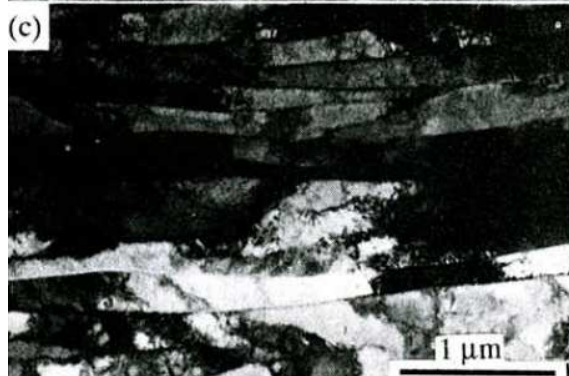
25%



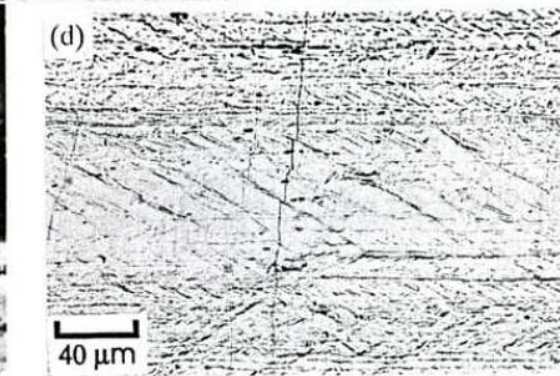
18%



98%



83%



mirobands

shear bands

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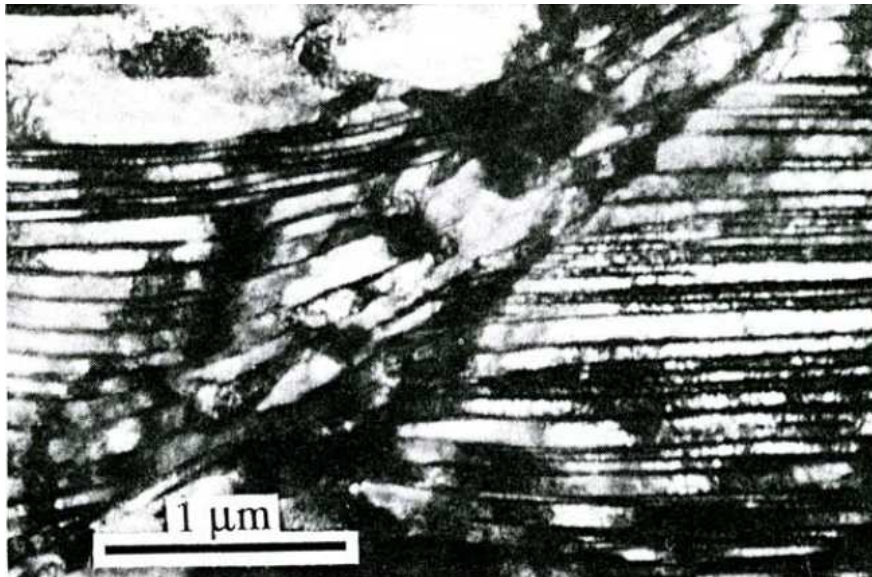
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Humphreys
& Hatherley,
1995



Shear bands in rolled metals

(110)[1-11] Cu single crystal
rolled 65% at 77K



Köhlhoff et al., 1988

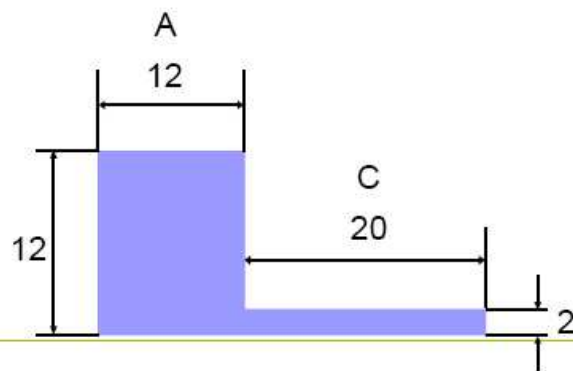
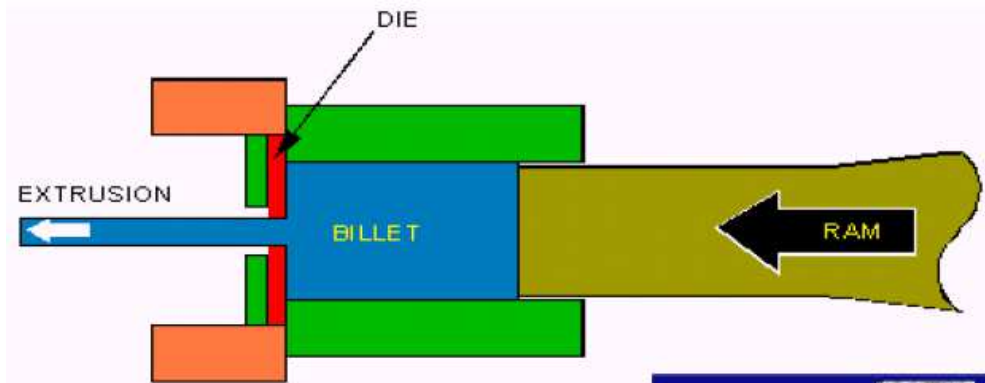
70:30 brass
rolled 50% at RT



Duggan et al., 1978

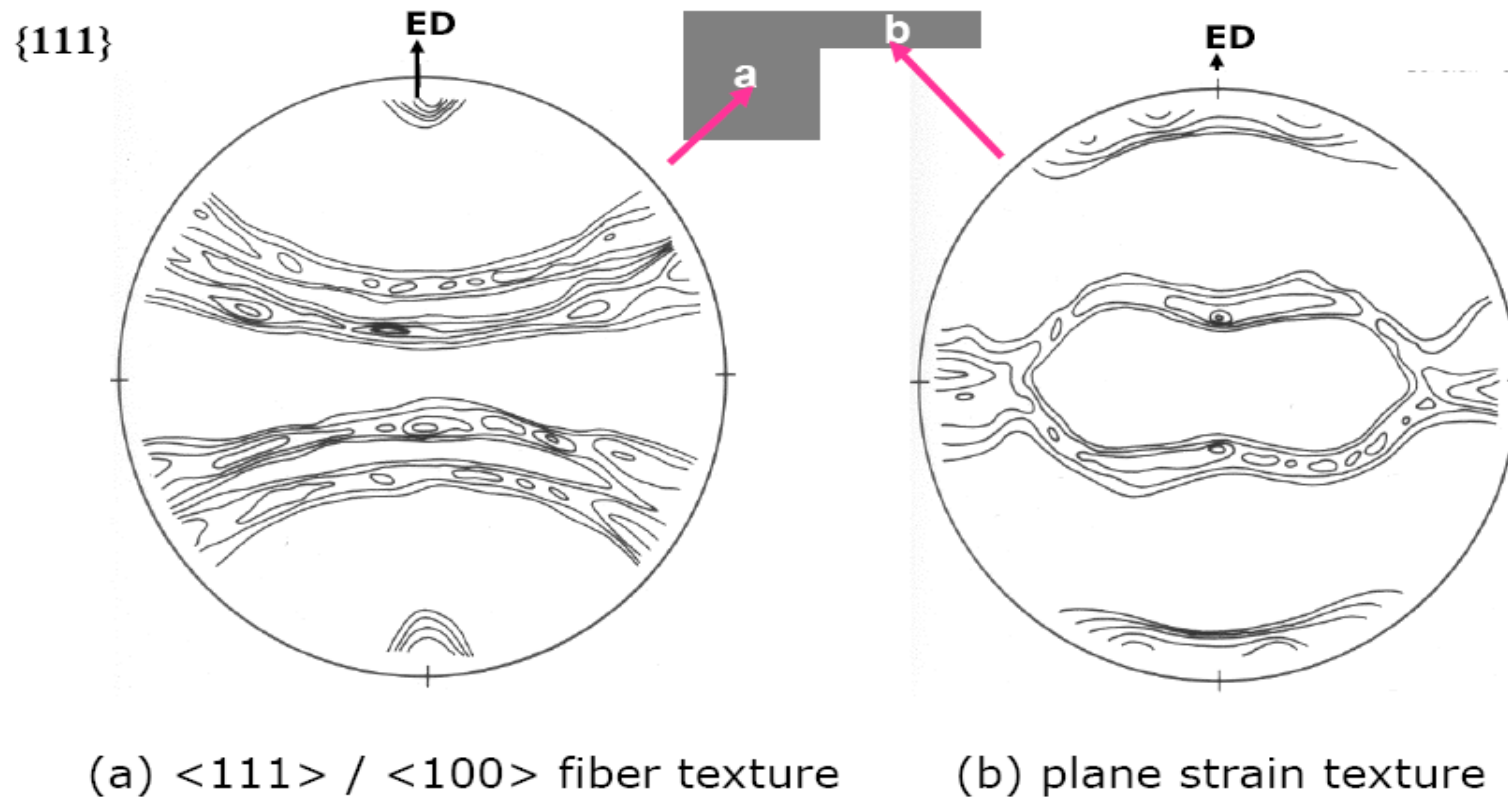


Extrusion of aluminium profiles



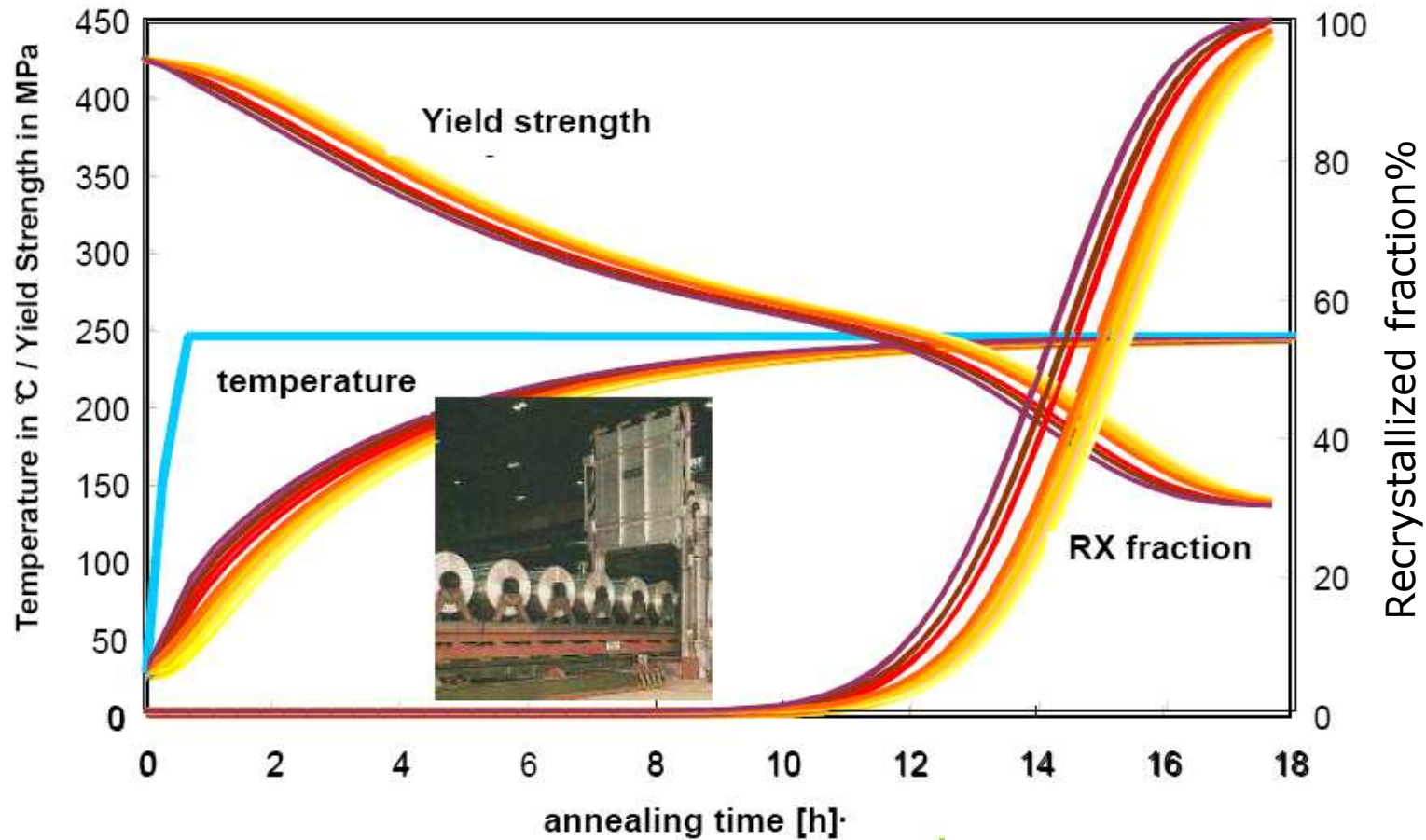


Texture variation in extruded Al alloy profiles





Temperature, recrystallization and strength evolution during coil annealing

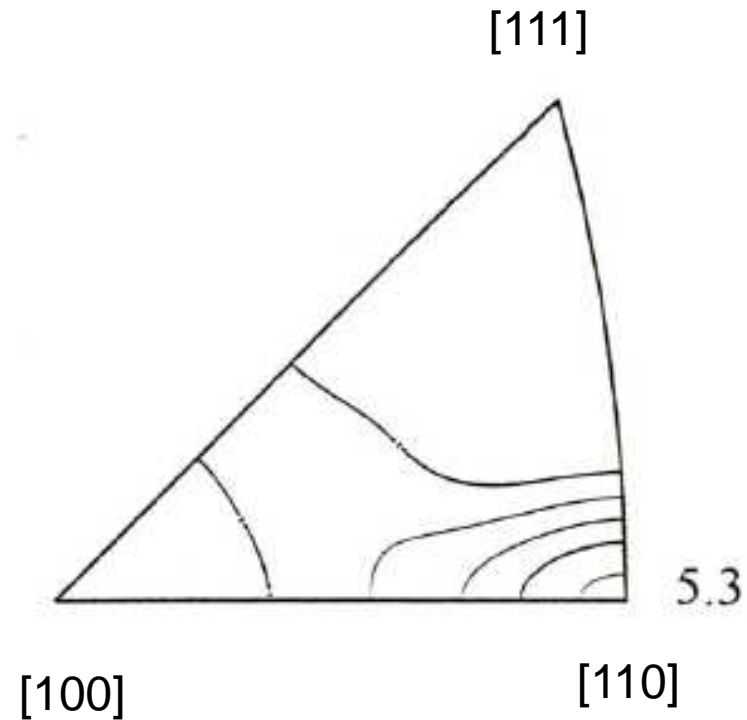
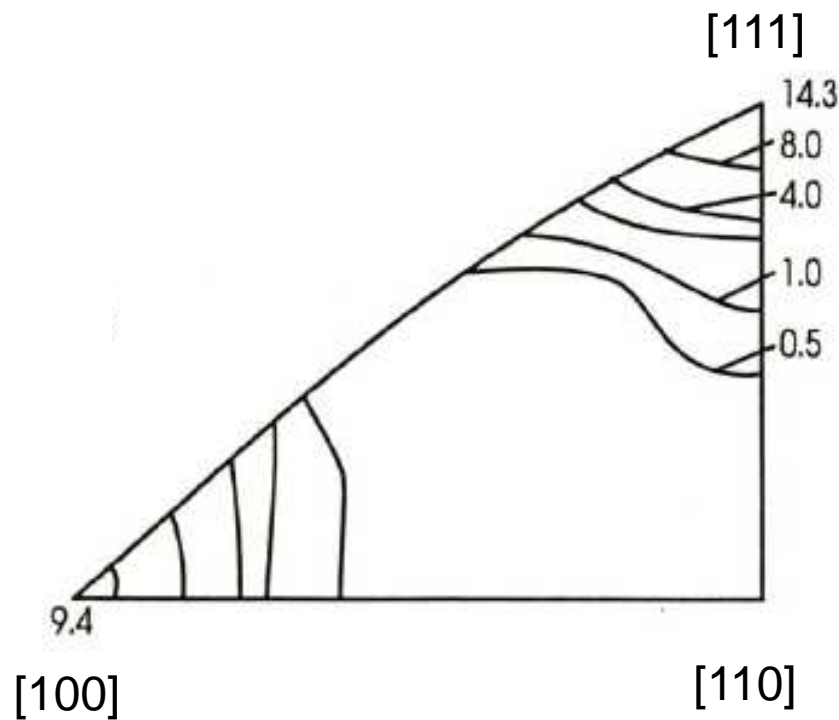




Compression and tension textures in a-Fe

compression

tension



Dillamore et al., 1974

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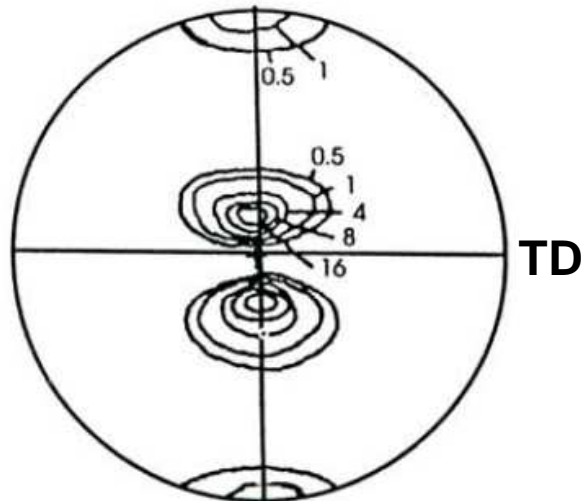
(0001) pole figures of rolled hexagonal metals

Zn

$c/a = 1.856$

high

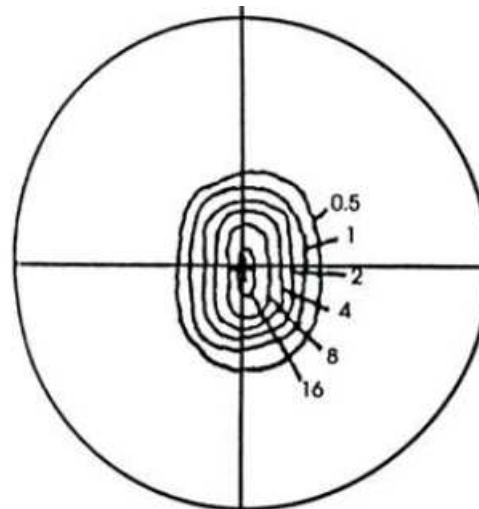
RD



Mg

$c/a = 1.624$

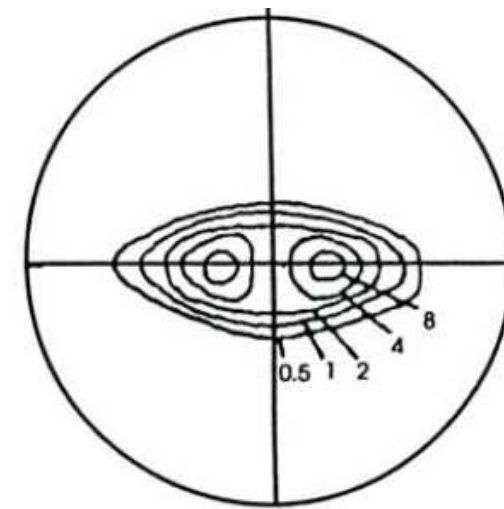
ideal = 1.633



Ti

$c/a = 1.588$

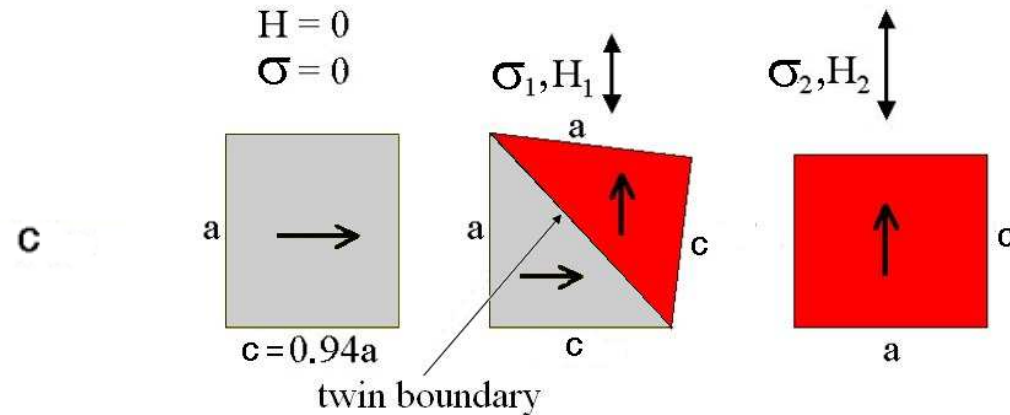
low



Hatherly & Hutchinson,
1979

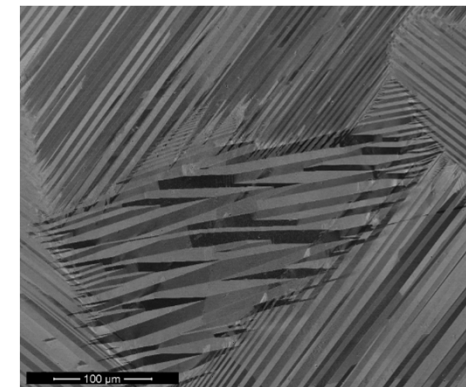
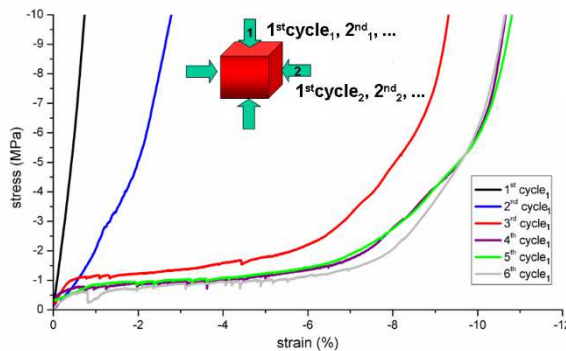


Magnetic field-induced strain



Requirements:

- high magnetocrystalline anisotropy
- highly mobile twin boundaries
 - Low twinning stress
 - Training process



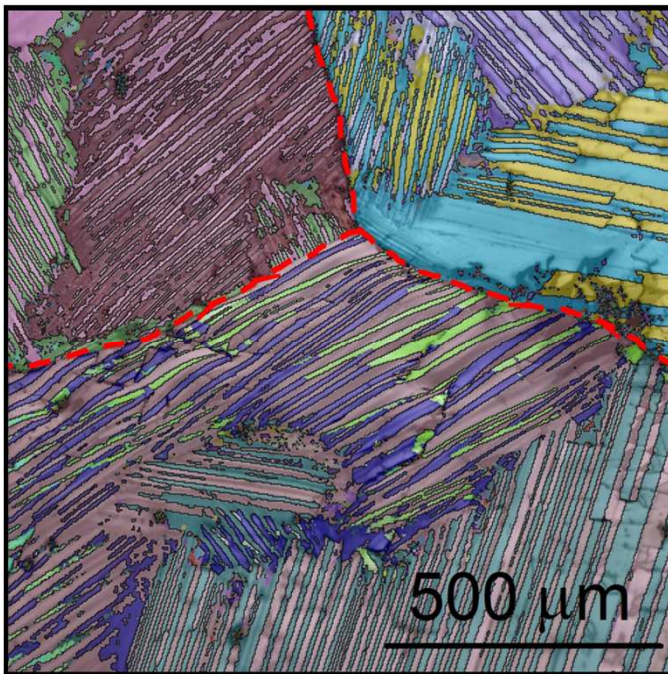
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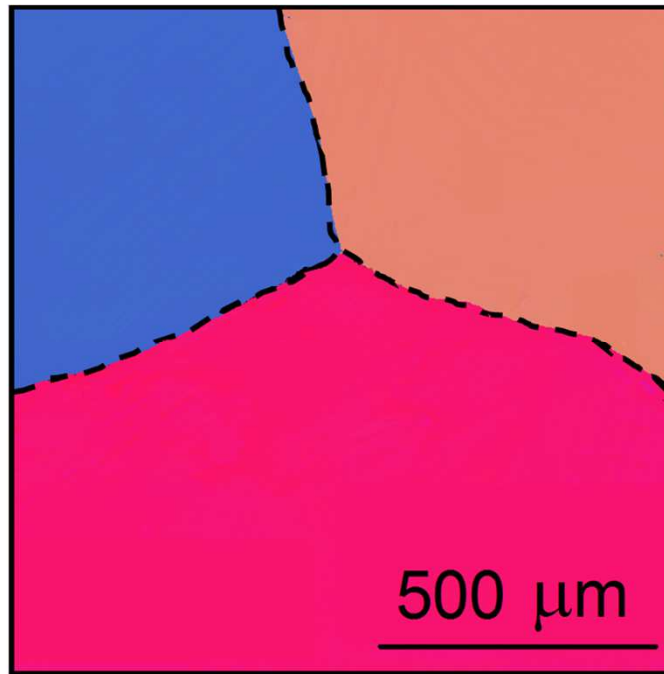
Texture inheritance

Martensite (RT)

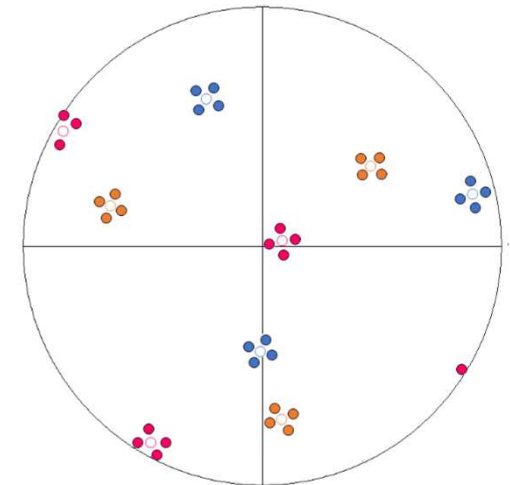


EBSD mapping, All Euler color coding

Austenite (110°C)



(001) pole figure



○ austenite
● martensite

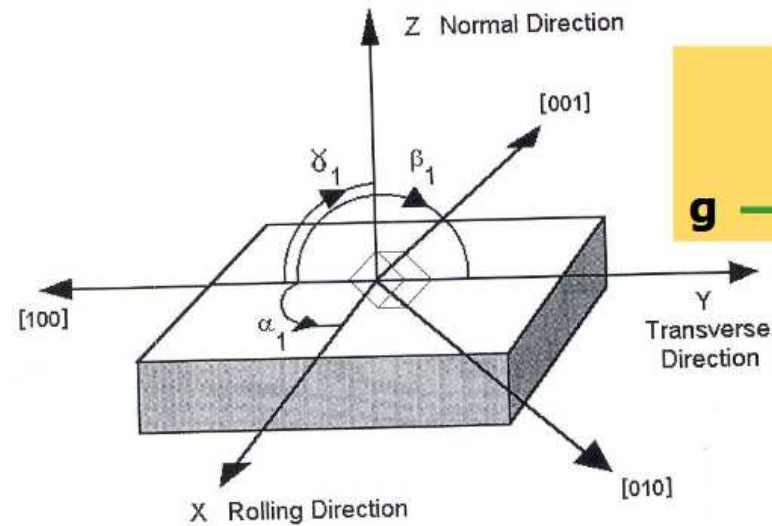


Orientation description

- $\{hkl\}\langle uvw \rangle$
- Pole figures
- Euler Angles
- Axis angle pair Rodrigues-Frank vector
- Quaternions



Orientation matrix



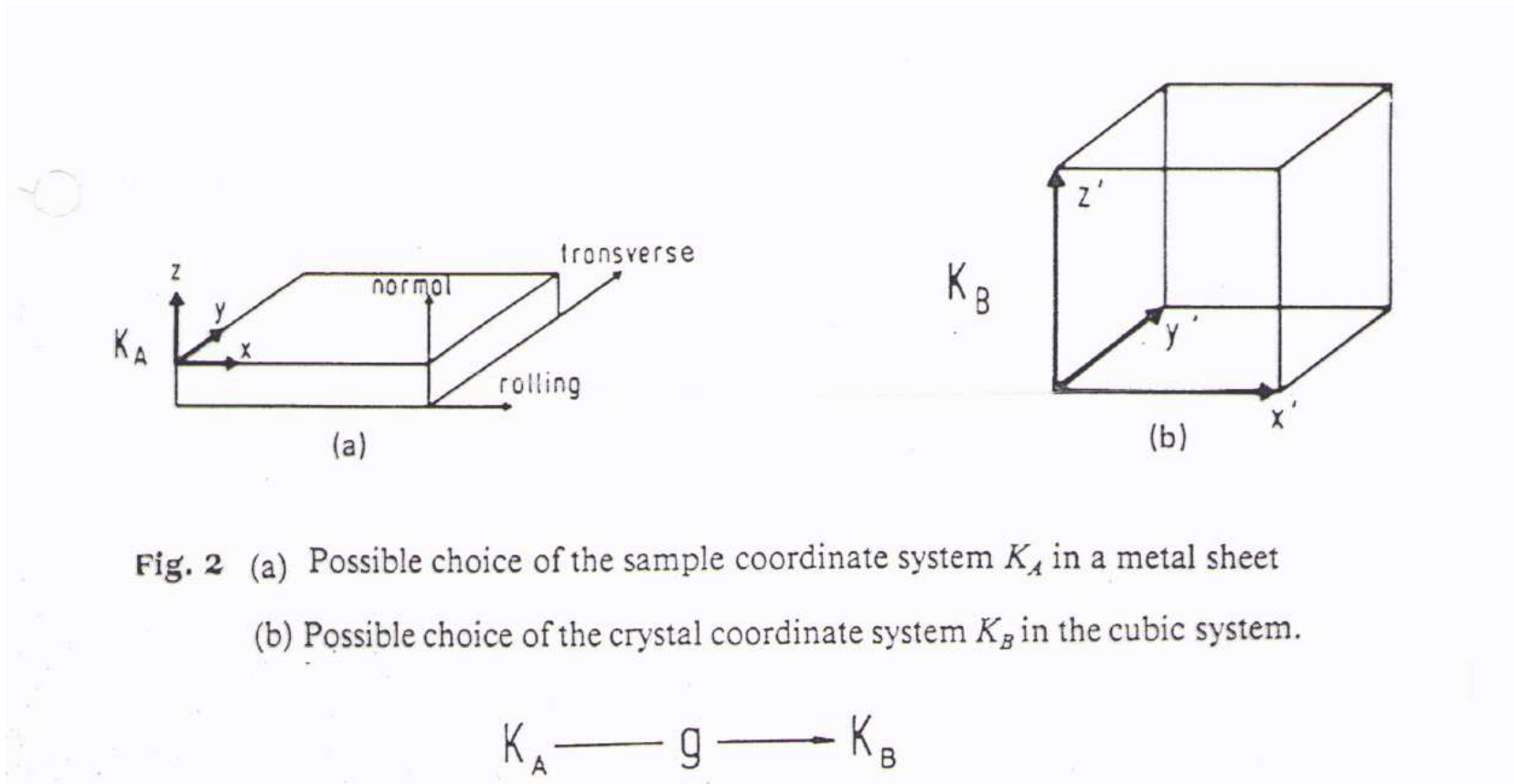
$$C_c = g C_s$$

g → orientation matrix

$$g = \begin{pmatrix} \cos \alpha_1 & \cos \beta_1 & \cos \gamma_1 \\ \cos \alpha_2 & \cos \beta_2 & \cos \gamma_2 \\ \cos \alpha_3 & \cos \beta_3 & \cos \gamma_3 \end{pmatrix} = \begin{pmatrix} g_{11} & g_{12} & g_{13} \\ g_{21} & g_{22} & g_{23} \\ g_{31} & g_{32} & g_{33} \end{pmatrix}$$

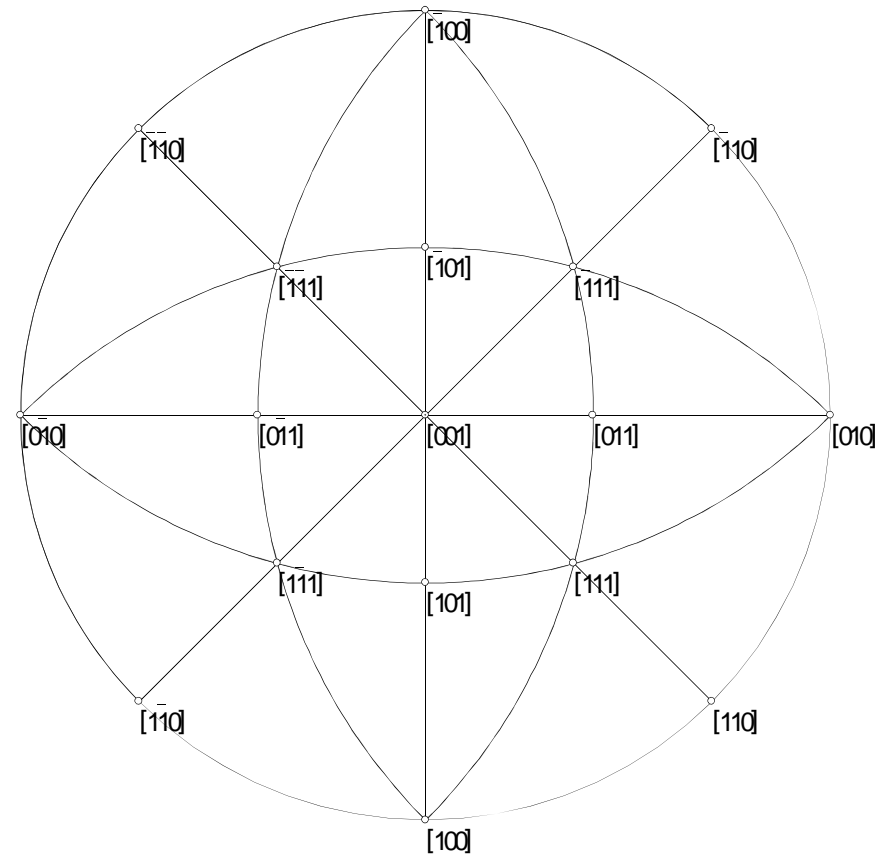
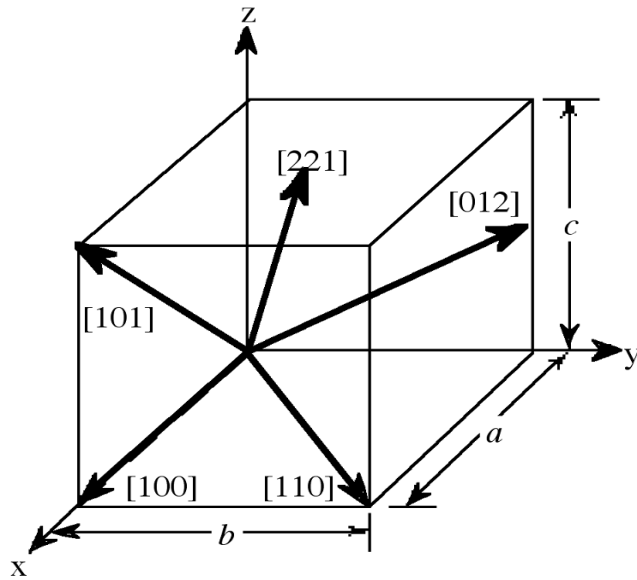


Coordinate systems





Crystallographic directions



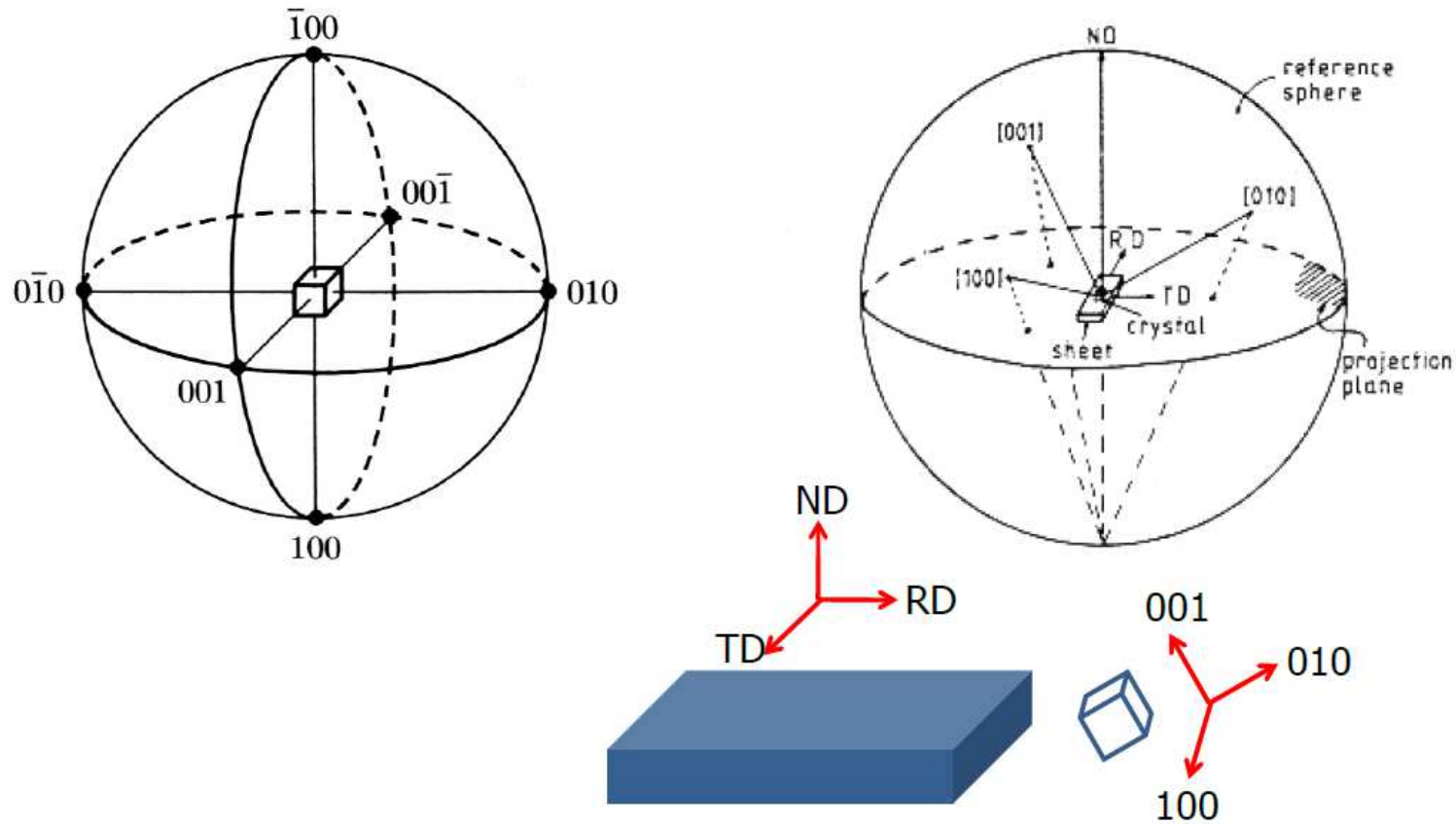
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Stereographic projection



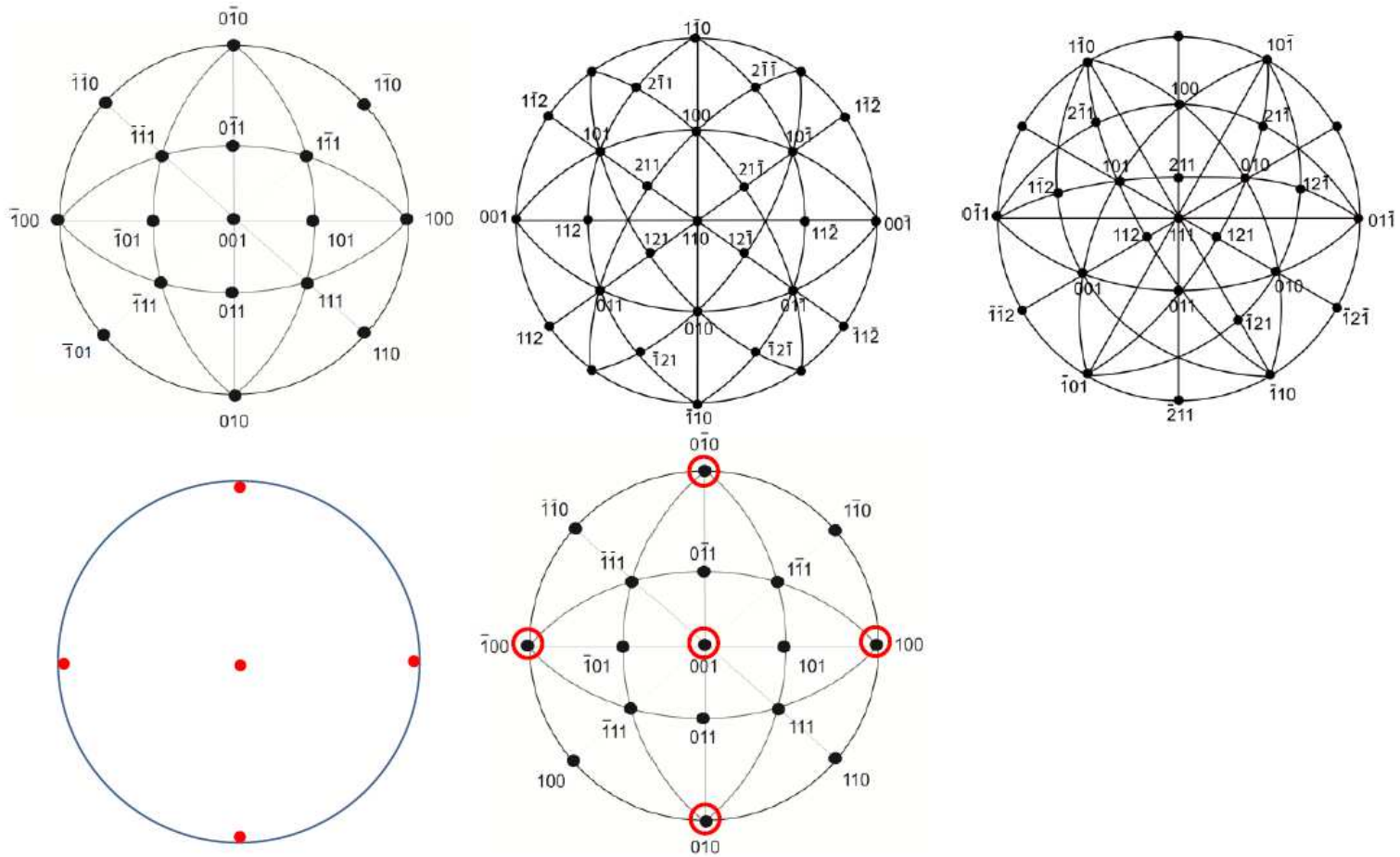
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Pole figures



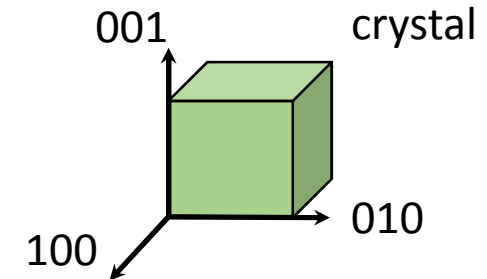
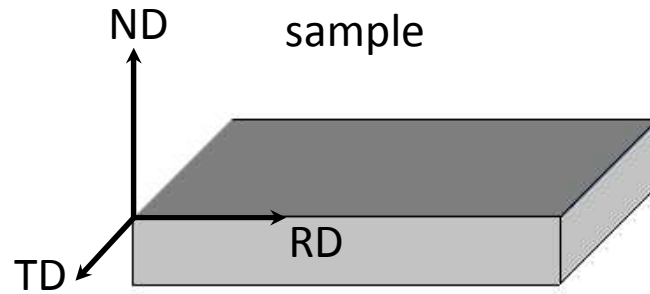
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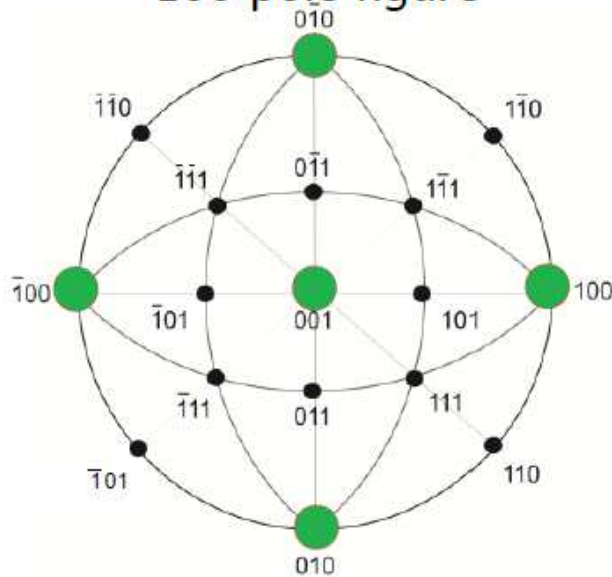
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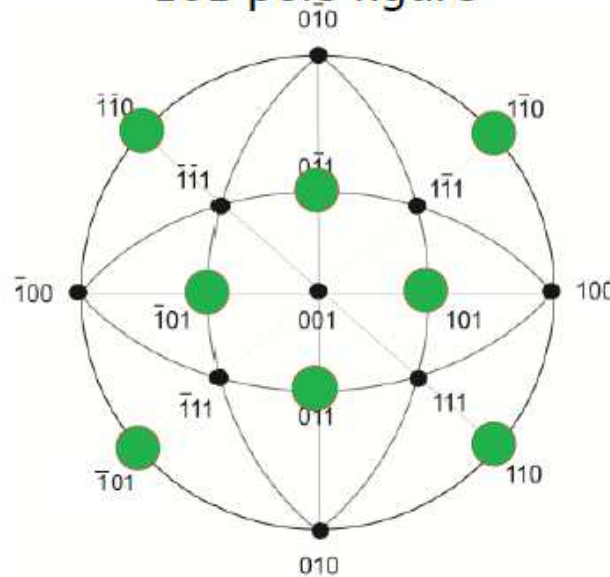
Coordinate systems



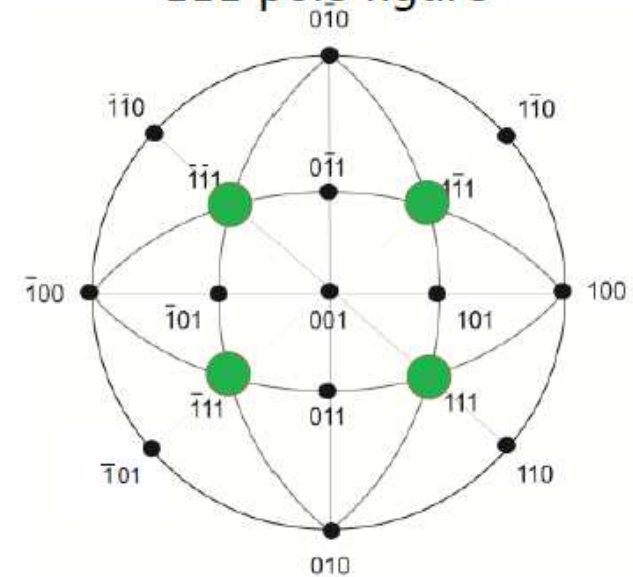
100 pole figure



101 pole figure



111 pole figure



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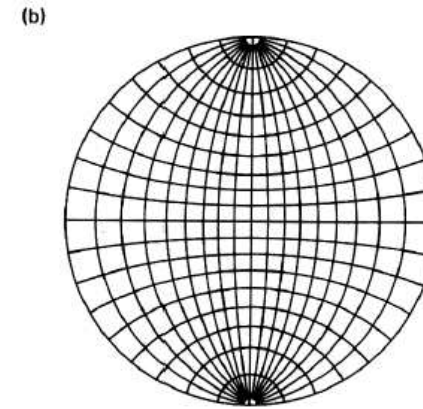
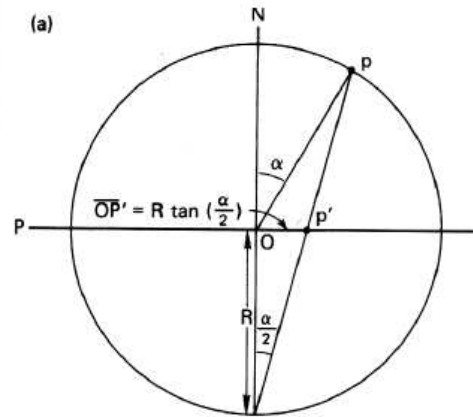
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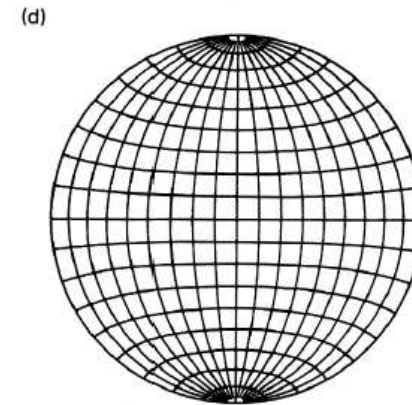
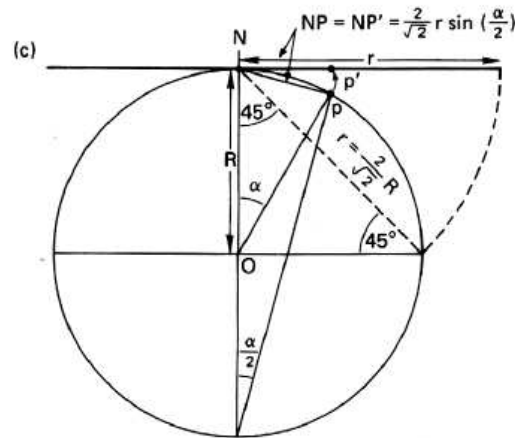


Stereographic projection

Angle true



Area true

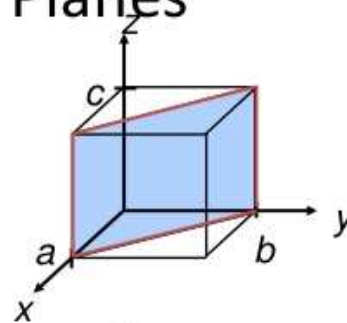




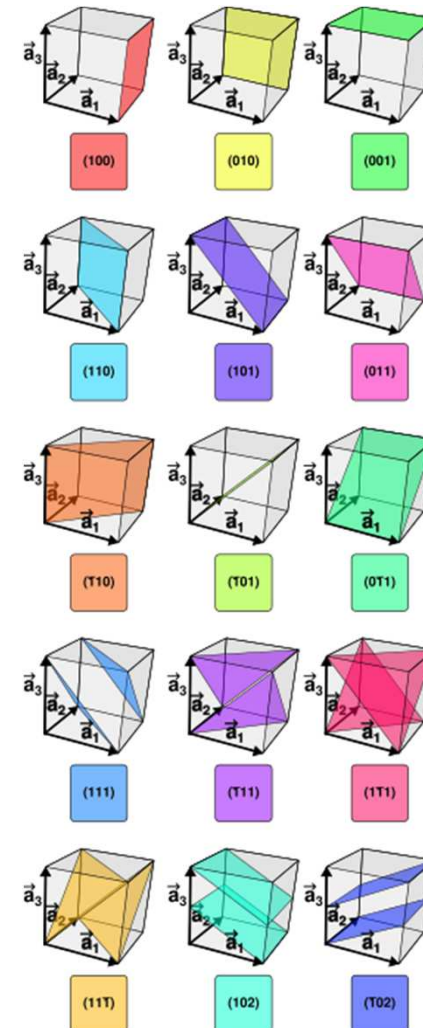
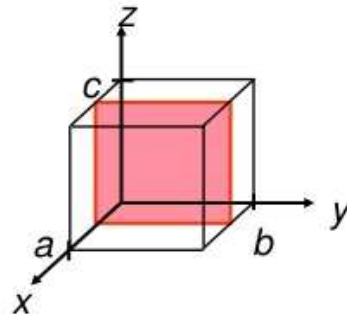
Crystallographic planes

Crystallographic Planes

example	a	b	c
1. Intercepts	1	1	∞
2. Reciprocals	1/1	1/1	1/ ∞
3. Reduction	1	1	0
4. Miller Indices	(110)		



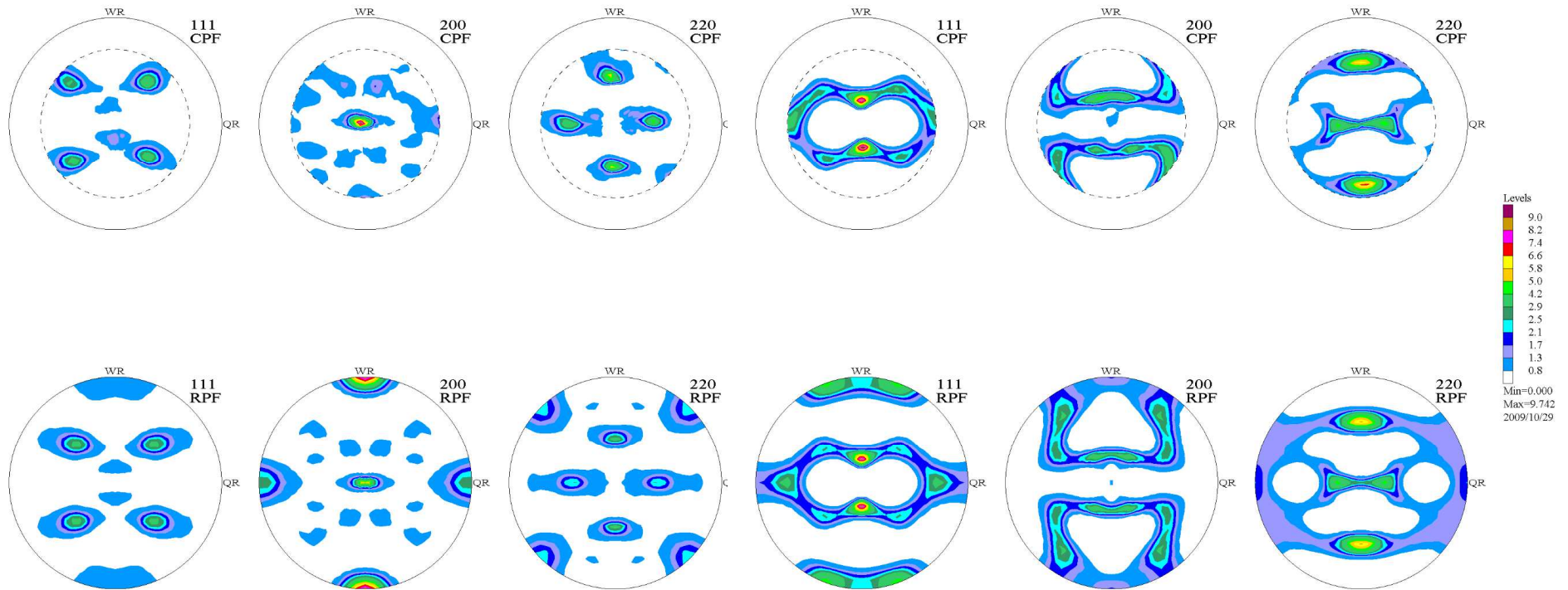
example	a	b	c
1. Intercepts	1/2	∞	∞
2. Reciprocals	1/1/2	1/ ∞	1/ ∞
3. Reduction	2	0	0
4. Miller Indices	(100)		



Experimental pole figures

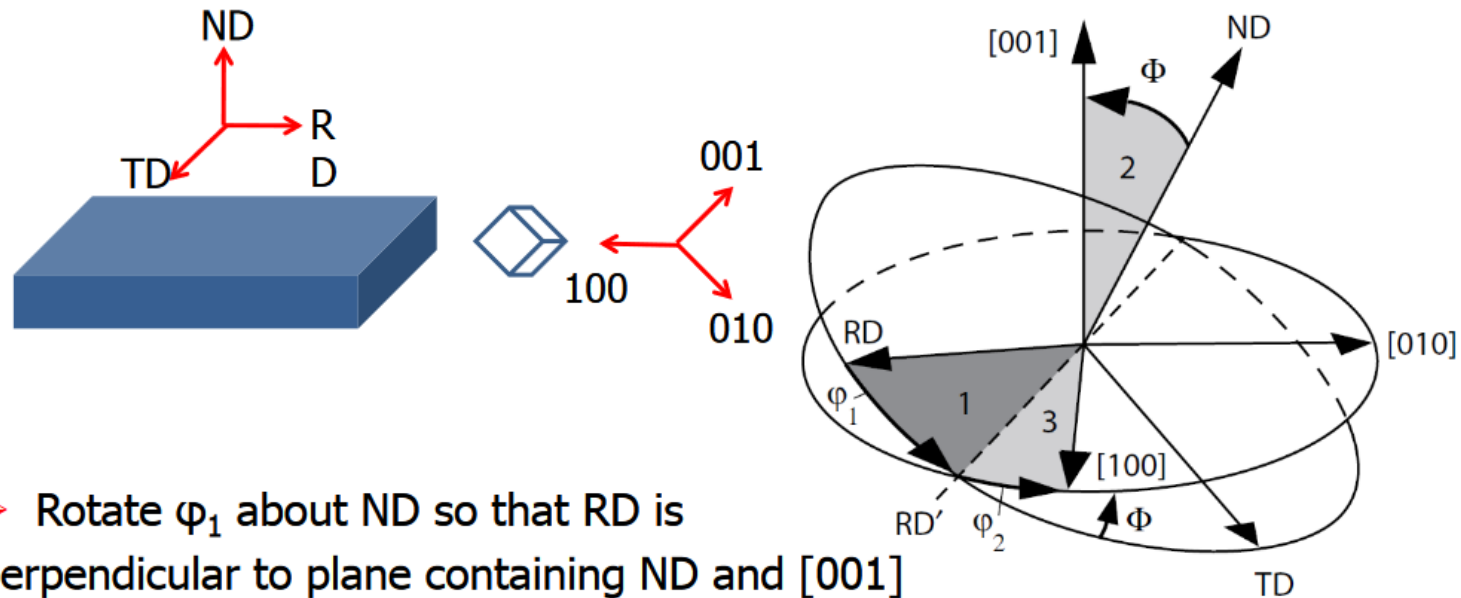
annealing

rolling





Euler Angles

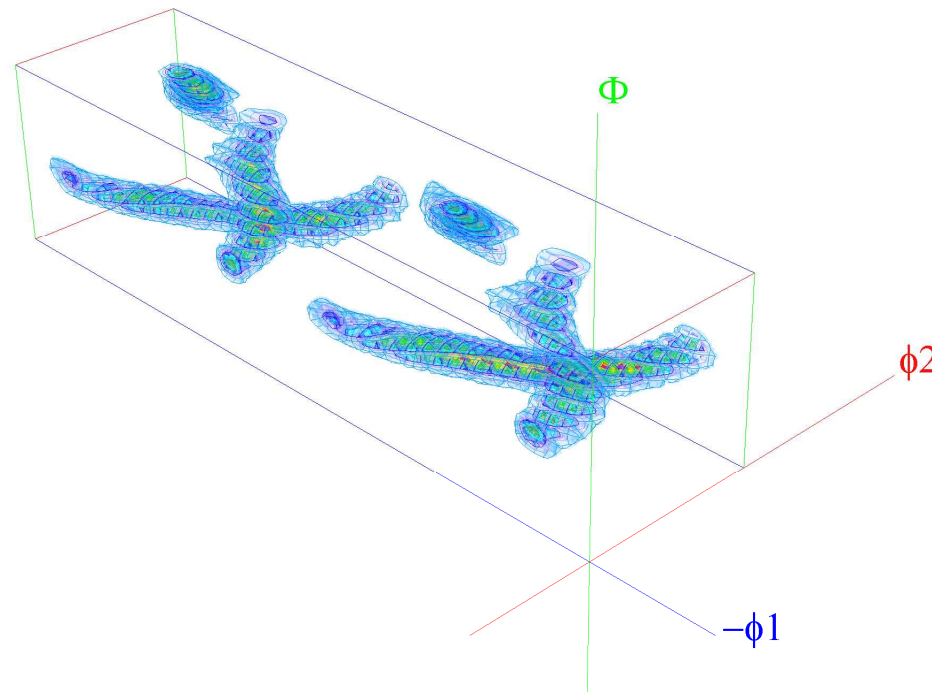


- Rotate φ_1 about ND so that RD is perpendicular to plane containing ND and [001]
 $RD \rightarrow RD'$ and $TD \rightarrow TD'$
- Rotate Φ about RD' so that ND and [001] coincide
 $ND \rightarrow [001]$ and $TD' \rightarrow TD''$
- Rotate φ_2 about ND so that crystal and sample frame coincide
 $RD' \rightarrow [010]$ and $TD'' \rightarrow [100]$



Orientation distribution function

$$\frac{dV}{V} = f(\varphi_1, \phi, \varphi_2) \frac{1}{8\pi^2} \sin \phi d\varphi_1 d\phi d\varphi_2$$

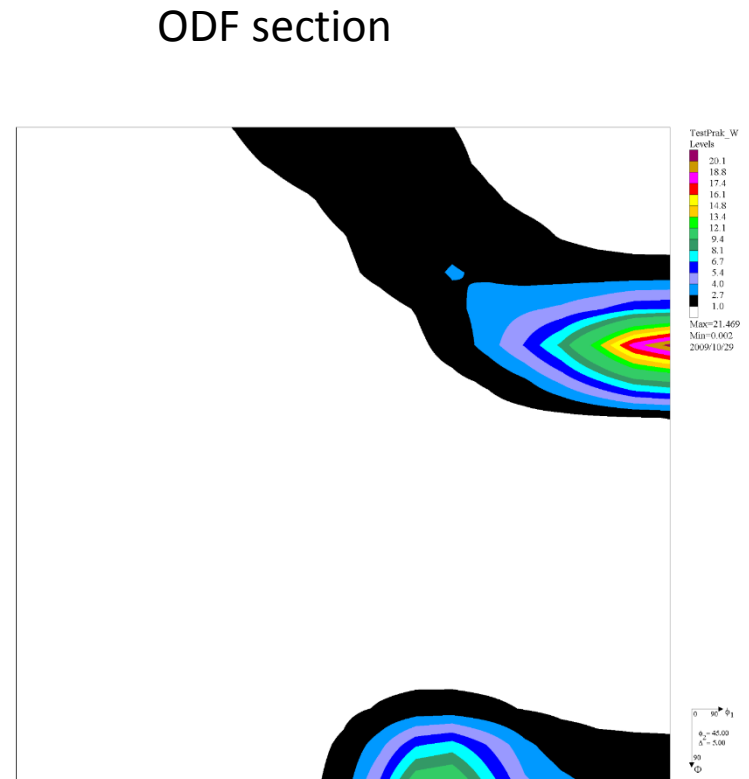
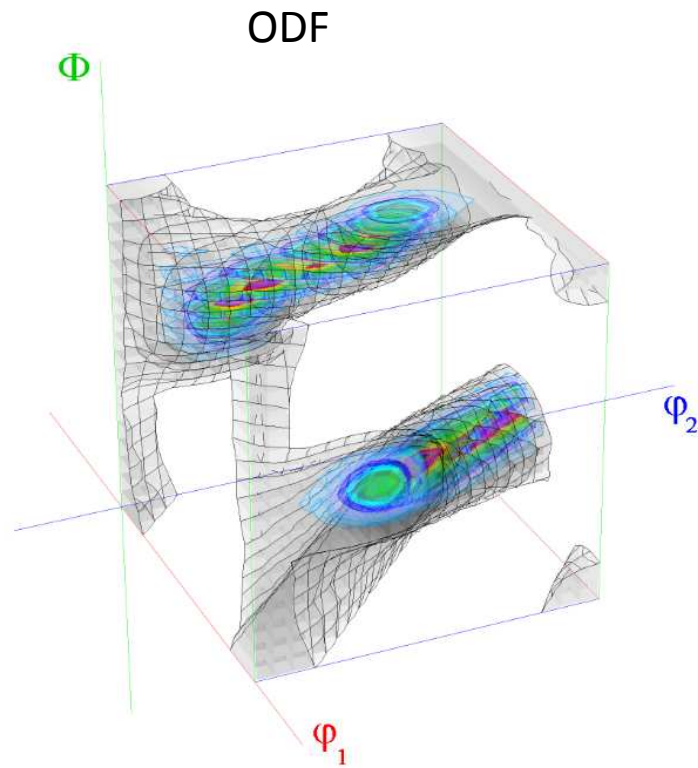


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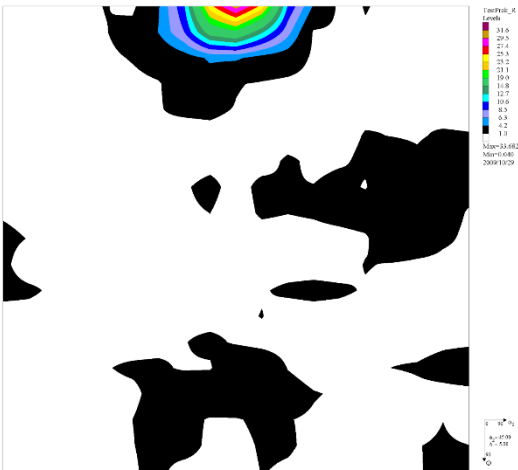
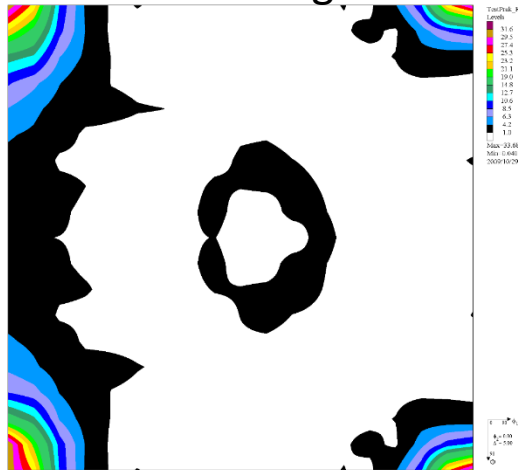
Orientation distribution function



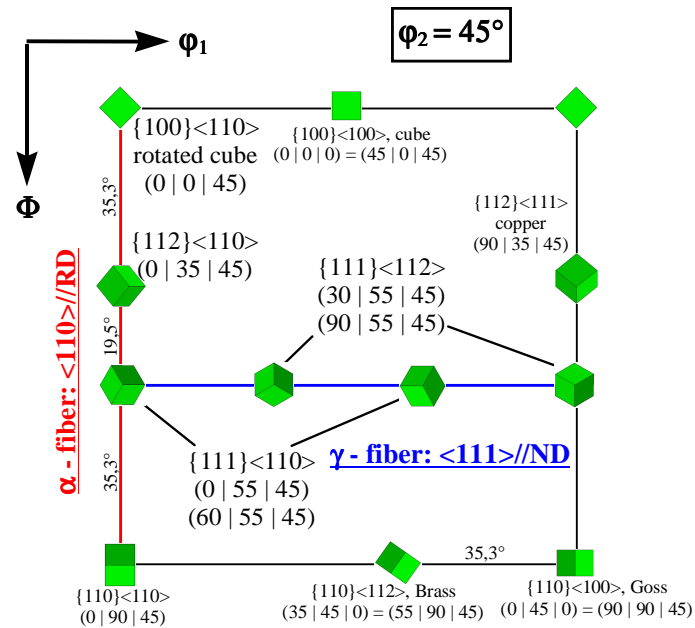
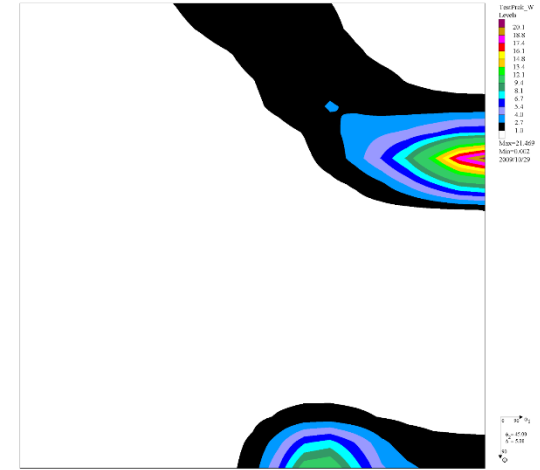
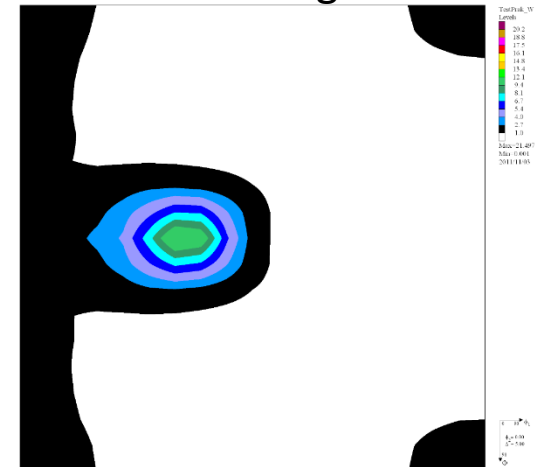


Key figure

Annealing



Rolling



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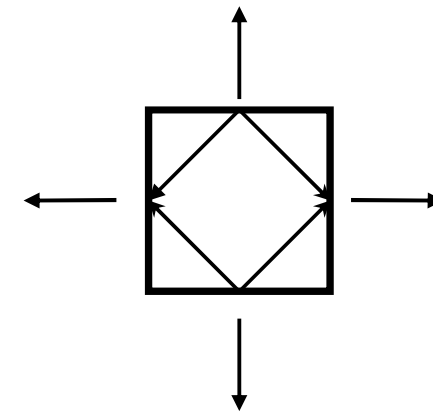
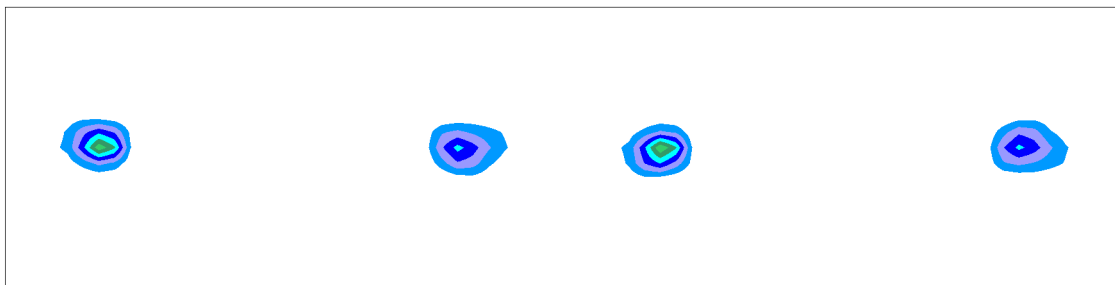
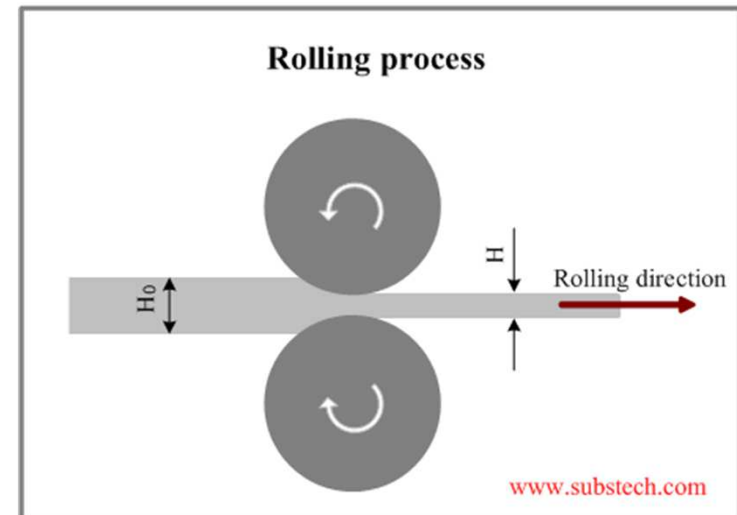
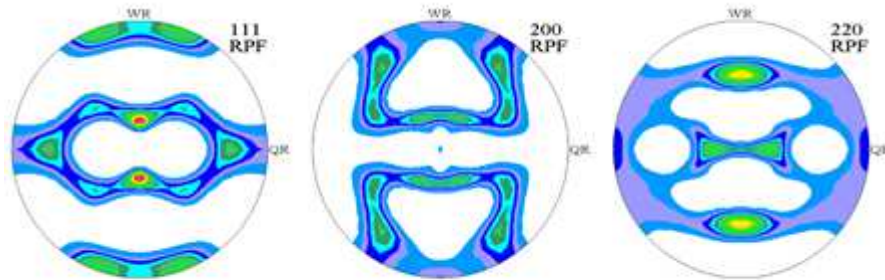
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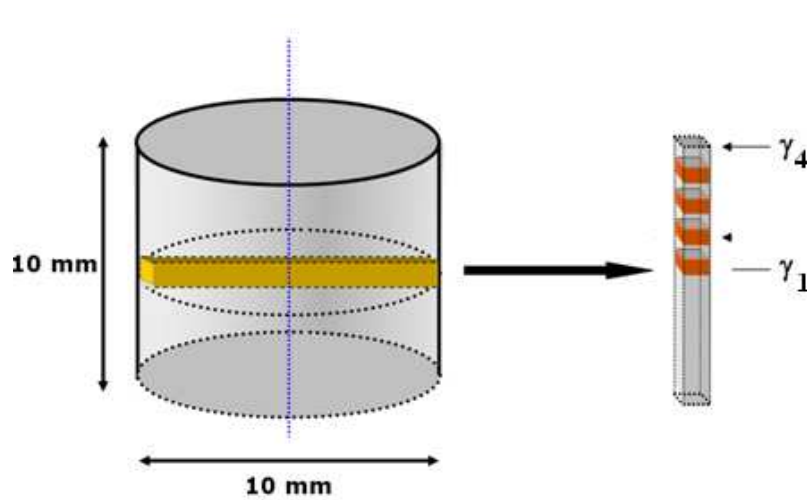
Sample symmetry (orthorhombic)

- Rolling



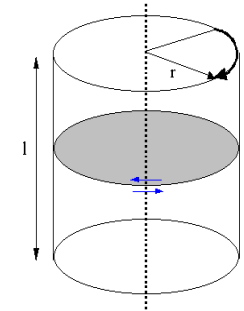


Sample symmetry – monoclinic



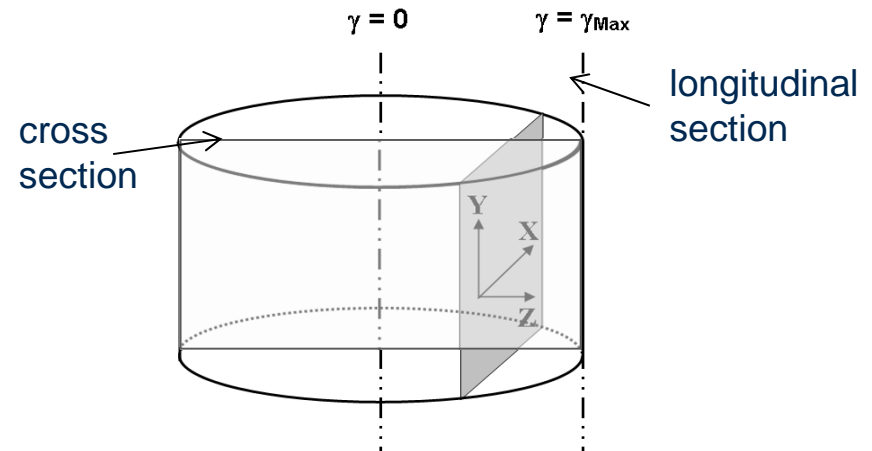
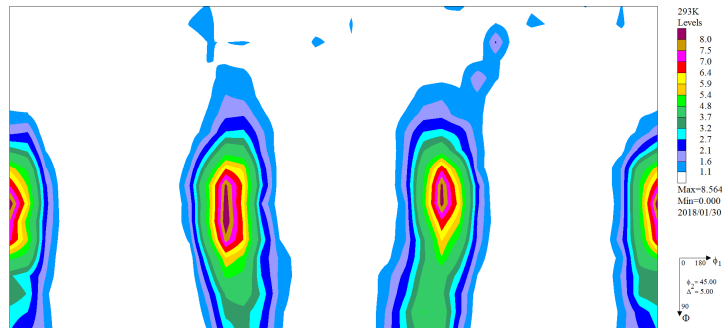
shear strain

$$\gamma = \frac{\Theta}{l} \cdot r$$



Microstructure – EBSD: longitudinal and cross sections

High Pressure Torsion (HPT)



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Sample symmetry - triclinic

ECAP

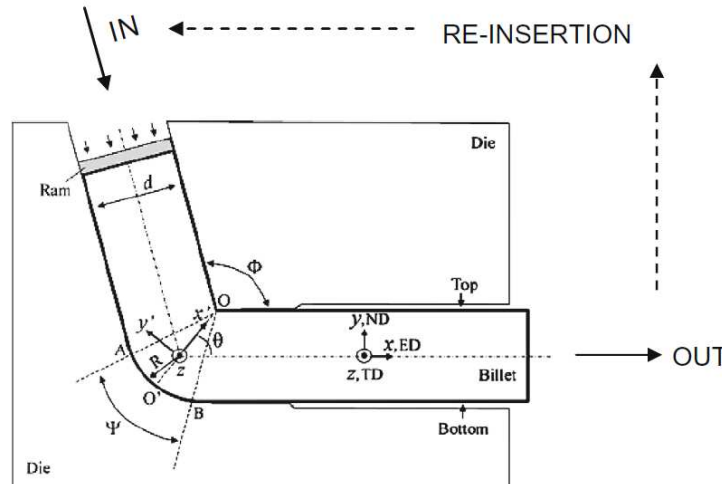
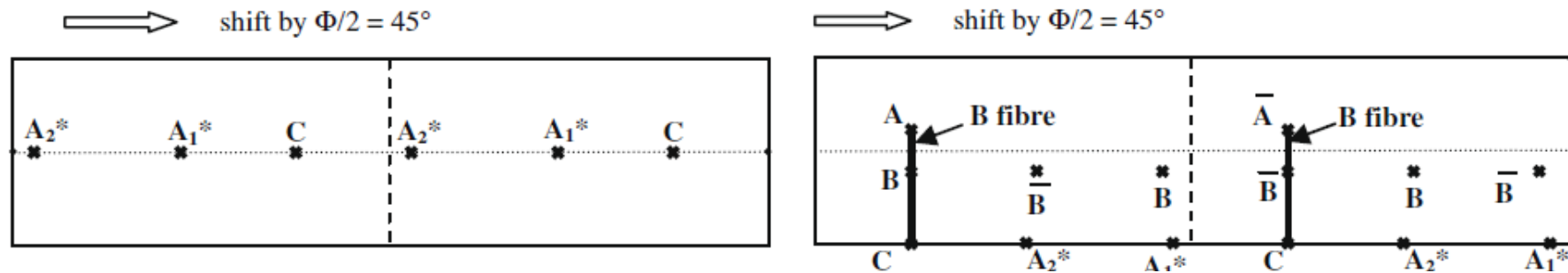


Fig. 1. ECAE die geometry and coordinate system employed in this paper [6].



I.J. Beyerlein, L.S. Tóth / Progress in Materials Science 54 (2009) 427–510

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